

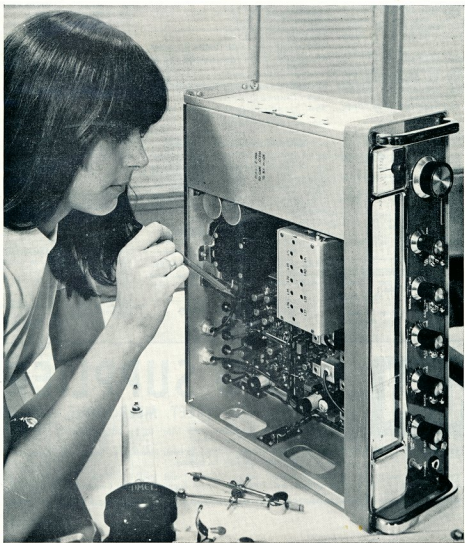
amateur radio

Vol. 39, No. 6

JUNE, 1971

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amateur radio

JOURNAL OF THE WIRELESS INSTITUTE OF AUSTRALIA. FOUNDED 1910



JUNE, 1971
Vol. 39, No. 6

Publishers:

VICTORIAN DIVISION W.I.A.
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Advertising Representatives:

TECHNICAL NEWS PUBLICATIONS
21 Smith St., Fitzroy, Vic., 3065. Tel. 41-4962.
P.O. Box 108, Fitzroy, Vic., 3065.

Advertisement material should be sent direct to the printers by the first of each month.

Hamads should be addressed to the Editor.

Printers:

"RICHMOND CHRONICLE," Phone 42-2419.
Shakespeare Street, Richmond, Vic., 3121.

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All matters pertaining to "A.R." other than advertising and subscriptions, should be addressed to:

THE EDITOR,
"AMATEUR RADIO,"
P.O. BOX 36,
EAST MELBOURNE, VIC., 3002.

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COVER STORY

The Eddystone model EC990S is a modern fully transistorised UHF receiver for AM/FM operation in the range 230-870 MHz. Designed for fixed or mobile operation, this unit has applications in meteorological service, radio astronomy, aerial investigation and in radio laboratories. In addition to audio and video outputs, a low impedance output at the i.f. of 36.5 MHz. is provided to drive ancillary equipment. Further information is available from R. H. Cunningham Pty. Ltd.

NOVICE LICENSING – AGAIN

The Federal Council at the 1970 Federal Convention divided equally on the question of whether or not the Wireless Institute of Australia should press for the introduction of some form of Novice licence in Australia. The Federal Council did, however, direct that the Federal Executive seek further information to be embodied in a report so that the question could be considered further. The Federal Executive sought the assistance of the New South Wales Division and accordingly a committee of that Division, under the chairmanship of Mr. Rex Black, VK-2YA, was formed. The report of the committee was received by the Federal Executive on 1st April, 1971, copied and posted to all Federal Councillors on 2nd April—that is exactly one week before the Federal Council met in Brisbane for the 1971 Federal Convention. The report has received universal praise; indeed the Federal Council formally recorded its deep appreciation of the work of the committee.

Yet, the Federal Council decided to defer decision on the matter. I know that very many people were interested in this question. Perhaps some will regret the decision to make no decision at this time. Perhaps it could be seen by a few as evidence of a thoroughly negative attitude. To draw such inference is, however, to be less than fair. First, let us look at the report. It raises, I believe, all the issues relevant to Novice licensing clearly and succinctly. In requesting such a report, the Federal Council was seeking as much factual evidence as possible upon which a decision could be based. The report provides this information. I have found this report most helpful on one of the most complex and difficult topics that have been considered in recent years.

In brief, the report recommends that the W.I.A. should seek the introduction of a "Novice" type of licence in Australia. This is necessarily a value judgment. There is no single fact that points unequivocally one way or the other. For example, the two countries with the highest ratio of Amateurs per head of population in the world are the United States of America and New Zealand. One has—the other does not have—Novice licences.

The report suggested, for discussion, that a Novice licence should be sought on the following basis:

- 1. A lower standard theory examination than that required for A.O.C.P. and A.O.L.C.P.

- 2. The same standard regulation examination as is required for the A.O.C.P.-A.O.L.C.P.
- 3. A five words per minute Morse test.
- 4. That the Novice licensee will use:
 - (a) A crystal controlled transmitter.
 - (b) Not more than 10 watts d.c. input.
 - (c) C.w. only.
- 5. The same age limit would be imposed as is imposed for A.O.C.P. and A.O.L.C.P.
- 6. A limited term licence only would be issued.
- 7. The licence would take with it the right to operate fixed, mobile or portable.
- 8. Special call signs would be allocated to Novice licensees.
- 9. A character reference would be required before a Novice licence is issued.
- 10. The Novice licensee would be permitted to operate on the following bands:—

1800 - 1860 KHz.
3505 - 3525 KHz.
7010 - 7050 KHz.
21030 - 21150 KHz.
28040 - 28200 KHz.

In addition, a number of other proposals were suggested. I have no doubt that this report will provoke spirited discussion. **That is exactly what it should do.** The report is printed as Appendix E to the Minutes of the Federal Convention. Your Federal Councillor has a number of copies. Please approach him for further details and please discuss the matter and express your view to your Federal Councillor and Divisional Councillors.

At the outset, I stressed the date the report was received by the Executive and circulated to the Federal Councillors. The committee, under Mr. Black, was appointed towards the end of 1970. It sought the views of many people and engaged in a volume of correspondence described by one Federal Councillor as "fantastic". That the committee achieved its object of producing a report prior to the Federal Convention is no mean feat. Perhaps, however, it is reasonable to ask whether the fact that a decision was deferred means that this effort was wasted. Emphatically, no. Formally, and particularly informally, the Federal Council engaged in a spirited and very deep discussion of the many issues involved. Had that report not been received in time for the Convention one of the most

useful discussions that have taken place in recent years would just not have occurred.

The introduction of a Novice licence system raises many issues fundamental to our hobby—the very purpose of the Amateur Service, the relationship of one type of licence with another, the virtues of quality as against the virtues of quantity are all relevant. Then, what do we set out to achieve with a Novice licence? How do we best do it? Do we take any different view of the two types of licence we already have? These are all equally relevant questions before we finally decide—if we do—to seek a Novice type licence and, even if we do so decide, the conditions of issue of such a licence raise question after question. No, the deferring of a decision was not evidence of negative thinking—rather it was a tribute to a magnificent report that deserves the fullest consideration and appreciation of the depth of a problem that, whilst in the past has been contentious, has not before been considered so completely. The deferring of the decision also gives each member the opportunity to re-consider his views and to take part in the formulation of one aspect of the Institute's policy that will undoubtedly and fundamentally affect our hobby for the future—whichever way the decision goes.

Finally, the matter does not have to wait another year. Your Federal Councillors are in regular communication with one another and with the Federal Executive. A decision can be made prior to the next Federal Convention if it appears that the pendulum previously finely balanced between "for" and "against" moves clearly in one direction or the other, thus answering the question "whether?". If the answer is "for" then the question "what?" (an equally complex question) must be answered. I believe, too, that given a consensus, that question, should it arise, can also be answered prior to the next Convention.

Mr. Black and his committee have made the way open for our organisation to make an informed decision on a topic that has troubled many people. A snap judgment would have pleased some, displeased others, depending which way it went. A considered judgment will, whichever way it goes, justify the enormous amount of work of the committee. This is a question that must fundamentally affect the future of our hobby. Please make sure that your voice is heard.

—MICHAEL J. OWEN, VK3KI,
Federal President, W.I.A.

HOME STATION ANTENNA FOR 160 METRES

Part Two—Vertical Polarised Antennas

J. A. ADCOCK,* M.I.E. (Aust.) VK3ACA

GENERAL

The basic medium frequency antennas are the quarter wave vertical (or Marconi) and the half wave vertical. An antenna having a better radiation in the horizontal direction is the five-eighths wave vertical, this behaves like half an extended double zepp. Both quarter wave and half wave verticals present a pure resistance load at the base. The quarter wave has a definite resistance of about 40 ohms which can be obtained from the formula. The half wave has a high resistance feed point at the ground. An antenna length other than a quarter wave or half wave has some reactive and some resistive component. The equivalent circuits of the loads of these antennas are shown in Fig. 3. In this article we are mainly considering antennas with a pole or leg length of less than a quarter wave and only verticals which are base fed against ground.

The quarter wave antenna when fed in series with the ground will be resistive only. For a short antenna the load can be looked on as a capacitance in series with a resistance. As the antenna is shortened the resistance will become smaller and the capacitive reactance will become larger (smaller capacitance). Because the effective series reactance becomes higher, the load requires a higher driving voltage, this voltage being largely out of phase with the current. In other words the load has a poor power factor.

This effective series reactance can be tuned with a variable series induct-

ance, and when this is done the resistance of the load is presented to the transmitter, the value of which is equal to the radiation resistance plus the loss resistance. For a short antenna the radiation resistance reduces with the square of the length of the antenna.

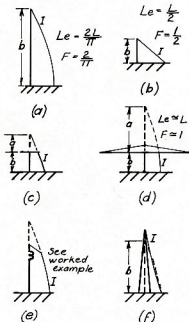


Fig. 4.—Showing the current distribution on some vertical antennas. (a) and (b) are used in the text to indicate electrical lengths of the component parts. L is the actual length of the radiating section. The effective length and the "form factor" are shown for some cases.

In some circumstances it may be desirable to consider the load as an equivalent parallel circuit as shown in Fig. 3. For a short antenna the equivalent parallel circuit will be one with a very high resistance and a high capacitive reactance. The equivalent series circuit is the one most commonly used. The conversion formula for parallel to series circuits is not given to avoid unnecessary complication. It is necessary to know the reactance to make the calculation. Series parallel conversion and reactance have been introduced later with references as an incidental.

As the antenna is made longer and approaches a quarter wave, the series reactance approaches zero or the parallel reactance approaches infinity, and the resistance in both cases approaches 40 ohms. As the antenna is lengthened beyond a quarter wave the series reactance increases and the series reactance becomes inductive. The series inductive reactance again approaches zero as the antenna length approaches a half wave and the resistance becomes a high value.

The distribution of current on a vertical antenna is shown in Fig. 4. The effective lengths of the antenna for the purpose of approximate calculation are also shown. Fig. 4a shows the current distribution for a quarter wave antenna, the distribution being approximately sinusoidal (Ref. 3). Fig. 4b shows the position for a short vertical. It will be noted that this distribution is approximately "triangular".

As pointed out already, a short antenna will necessarily have a low feed point resistance and therefore a large current. The driving voltage will also be high due to the high series reactance. An equivalent series circuit of a complete tuned short antenna is shown in Fig. 5. The constants are considered lumped. From the circuit it is obvious that if the losses are to be minimal the radiation resistance should be high and steps should be taken to reduce losses. In the antenna in Fig. 4b the current will be maximum at the bottom and zero at the top. As a result, current at the feed point is twice the average current and therefore the radiation resistance is low, also a large base loading inductance is required to tune the antenna.

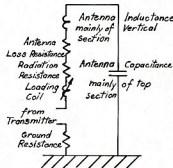


Fig. 5.—Showing a series equivalent circuit of the whole antenna. The main parts are shown lumped.

A much better distribution of current is achieved by "top loading", shown in Figs. 4c, d, and e. The top load can be made large enough so that the current in the vertical section is practically constant over the length considered. In fact the top can be made large enough so that the antenna will resonate.

Large capacitive top loading has the following advantages:

1. The current distribution in the radiating section is optimum, resulting in maximum radiation resistance.
2. Minimum tuning inductance is required.
3. The large capacitive top ensures minimum voltage stress to produce the necessary electrostatic field, hence minimum tendency to corona.

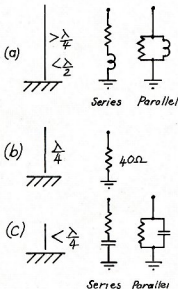


Fig. 3.—Showing the antenna together with the equivalent series and parallel circuit of the load when the antenna is fed in series with the ground.

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Initially in this discussion the top is considered to be symmetrical and therefore would radiate very little since currents flow in opposite directions and produce a largely cancelled field.

A symmetrical antenna with a straight wire top is very ancient and goes under the name of "T". The top load, however, can take several other forms, e.g., an umbrella, several horizontal radials, a flat disk, an inductively loaded whip, a cylinder or a sphere. An antenna with a single top wire at right angles is known as an "inverted L". A "sloping antenna" is also a vertical and these will be dealt with in a separate section.

The top loading will have an effect on the antenna like an extra length of wire vertically (non-radiating). This equivalent effective vertical is shown as length "a" in Figs. 4c, d and e, and the vertical radiating section is shown as length "b". The current distribution over the real and virtual part of the antenna in all cases except Fig. 4f is close to sinusoidal (Ref. 3). The shortening effect of a tapering antenna is only illustrated here and is not analysed.

CALCULATIONS FOR VERTICAL ANTENNAS

Radiation resistance of a vertical antenna when fed in series with the ground is given by—

$$R_a = \frac{1580 L_e^2}{\lambda^2} \dots \dots (1)$$

where L_e = the effective length of the antenna.
 λ = wavelength.

Fre- quency	λ metres	λ feet	$\lambda/4$ feet
1.8	166.7	546.8	136.7
1.825	164.4	539.3	134.8
1.85	162.2	532.0	133.0

Since we are considering the vertical component only any horizontal radiation resistance can be considered part of the loss. This value is usually small. In the graphs given here the electrical length of the antenna is taken as $\lambda/4 = 1$. This was considered to be simpler for calculation than $\lambda/4 = 90^\circ$. If calculations are made from tables, angular lengths would have to be used. In the examples given here no reference is made to velocity factor or end effect as these values should make a small difference only.

The effective length of the antenna and the form factor of the current distribution are as defined earlier.

$$F = L_e \div L$$

$$L_e = F \times L \dots \dots (2)$$

where F = form factor.

L = actual length over which the current distribution is being considered.

The vertical component of the antenna, the length over which the vertical current distribution is considered, is usually the gap between the top load and the ground.

Also—

$$F = \frac{\text{Average Current}}{\text{Base Current}} \dots (3)$$

$$\text{Average Current} = \frac{\text{Area under Current Distribution Graph}}{L} \dots (4)$$

In the case of a triangular distribution of current (Fig. 4b), the average current must be half that of the base current. Therefore it would radiate the same power as a wire of half the length carrying a constant current equal to the base current ($F = \frac{1}{2}$). In the case of Fig. 4d, the effective length is equal to the actual length ($F = 1$).

The form factor for a quarter wave is $2 \div \pi$, as shown in Fig. 4a. The true form factor for a radiating section of wire is given below.

From equations 3 and 4:

$$F = \frac{\int_{x=0}^{x=L} i \, dx}{L I}$$

where i = current at distance x from the end of the antenna.

L = length of the radiating section being considered.

I = base current.

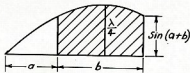


Fig. 6.—Illustrates the method used for equation 5.

Consider Fig. 6. The length "a" is the equivalent electrical length of the top (not necessarily the actual length) and length "b" is the electrical length of the radiating section. The current distribution in the wire is sinusoidal. From the equation the electrical length L must be taken in radians and equals length "b".

$$F = \frac{\int_{x=a}^{x=b} \sin x \, dx}{\text{radian } b \times \sin(a+b)} = \frac{\cos a - \cos(a+b)}{\text{radian } b \times \sin(a+b)} \dots \dots (5)$$

a and b can be taken as the angular length $\lambda/4 = 90^\circ$ and the figures taken

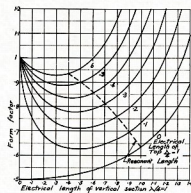


Fig. 7.—Curves of "form factor" against electrical length of the radiating section for various lengths of top load.

from tables. Note that if $(a + b)$ is greater than 90°

$$\cos(a + b) = -\cos[180 - (a + b)].$$

Calculations from equation 5 are shown plotted in Fig. 7, and using equation 6 below, Fig. 8 was plotted.

Taking:

$$\text{electrical length} = L \div \lambda/4$$

and from equations 1 and 2

$$R_a = 98.75 (\text{elect. length} \times F)^2 \dots (6)$$

Example for a simple quarter wave vertical:

$$R_a = 98.75 \times (1 \times 0.636)^2 = 39.9$$

It must be pointed out that this method of calculating radiation resistance is a simplified method and is only correct if the radiating section of the antenna is short. If it is near a quarter wavelength or longer the radiation resistance will be less by a small amount, however the results given by the formulae and graphs shown here should be sufficiently accurate within the range shown.

According to the formula, as the antenna approaches a half wavelength the radiation resistance approaches infinity. This is obviously erroneous. If the total electrical length of the antenna is more than 1.4 of a leg length of a quarter wave, the formulae should not be used. The radiation resistance at the base of a half wave vertical cannot be accurately calculated but would be in the order of several thousand ohms.

A choice of methods for determining the form factor of the current distribution on an antenna has been given and these are summarised as follows:

1. If the current distribution conforms nearly to the standard forms shown in Fig. 4, these may be applied. F for a short vertical = 0.5 and F for a heavily loaded vertical = 1, the latter may not be sufficiently accurate on 160 metres.
2. If the current distribution curve is known, equations 3 and 4 can be applied and the areas under the current curve determined graphically or by measurement.
3. By application of the graphs or equation 5.

Effective Electrical Length of Top Load

This matter created some discussion as some authorities state that in the case of a "T" the effective length is equal to half the length of the top, that is, the "inverted L" section only and other authorities seem to leave the matter open.

The following would appear to be correct (Ref. 4):

1. With an "inverted L" the effective electrical length of the top is equal to the actual electrical length.
2. The electrical distance of the point being considered on the antenna from the current or voltage point (virtual or otherwise) is dependent upon the reactance component at that point.
3. The antenna can be considered as a wire with approximately 600 ohms characteristic impedance.

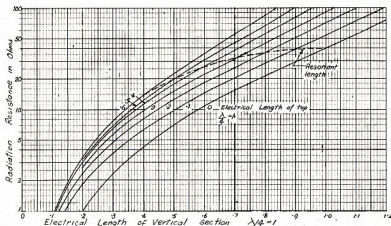


Fig. 8.—Radiation resistance of a vertical against height for various equivalent lengths of top load.

4. The no-load reactance curve for an unloaded 600 ohm line is near enough to correct except close to the voltage loop.

5. At the junction of the "T" the reactance load of each half will add in parallel to produce a reactance of half that of the individual line.

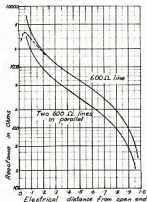


Fig. 9.—Curves for the open circuit capacitive reactance of a 600 ohm line or antenna. The lower curve represents the reactance when two lines are joined in parallel, such as the junction at the top of a "T" antenna. The short dotted curve at the top left shows the deviation in effective series reactance when the line is loaded with an s.w.r. of 12. For higher s.w.r.'s the deviation will be even less.

Fig. 9 has been drawn based on wire and two wires in parallel. (The mutual capacitance and inductance between the wires was not taken into account.) From these graphs, Fig. 10 was plotted to determine the equivalent electrical length of two lengths of wire (a "T" top).

Efficiency of Antenna

The radiation resistance of the antenna is dependent mainly upon the configuration and not on the loss resistance. The actual resistance of the load of the antenna will equal the radiation resistance R_r plus the loss resistance R_l .

$$\text{Power radiated} = I^2 R_r$$

I = the current at the feed point.

Power input to the antenna = $I^2 R$
 R = the total resistance of the load
 $R = R_r + R_l$

Since R is an unknown quantity
 $R = W \div I^2 \dots \dots (7)$
 W = power input to antenna.

The power input to the antenna can be estimated from the final input. For a class C amplifier, 70% efficiency is reasonable. For a sideband rig, the manual should give sufficient information to estimate the power output.

$$\begin{aligned} \text{Radiation efficiency of antenna} &= \frac{\text{power radiated}}{\text{power input to antenna}} \\ &= \frac{I^2 R_r}{I^2 R} \\ &= \frac{R_r}{R} (\times 100\%) \dots \dots (8) \end{aligned}$$

R_r is found from graphs or calculation and R is found from equation 7. It is possible to use a Q meter or a bridge to obtain the load resistance but these were found to have certain difficulties as referred to in the discussion. The r.f. ammeter should be of the thermocouple type and should be checked against an ammeter at 50 Hz.

It may be useful to obtain the loss resistance.

$$R_l = R - R_r \dots \dots (9)$$

In a grounded vertical antenna, R_l will be mainly ground resistance.

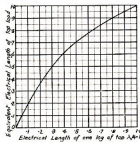


Fig. 10.—The length of one leg of the top of a T is plotted against the length of a single wire which would have the same effect.

Worked Example

A "T" antenna is 45 feet high and has a 66 ft. flat top. With 100 watts input to the final the antenna current is 1.8 amps.

Electrical length of half top ($\lambda/4 = 1$) $\dots \dots = 0.245$
 Equivalent electrical length of top (Fig. 10) $\dots \dots = 0.43$
 Electrical length of vertical section $\dots \dots = 0.332$
 Form factor (Fig. 7) $\dots \dots = 0.86$

From equation 6
 $R_r = 98.75 \times (0.86 \times 0.332)^2$
 $= 8.0 \text{ ohms.}$

From equation 7
 $R = \frac{100 \times 0.7}{1.8^2}$
 $= 21.2$

Efficiency of antenna = $8 \div 21.2$
 $= 0.38 \text{ or } 38\%$

$R_l = 21.2 - 8.0$
 $= 13.2 \text{ ohms}$

probably mainly ground resistance.

THE CENTRE LOADED VERTICAL

The effect of an inductance in a vertical is to increase the capacitance loading of the top from the point of view of the bottom, Fig. 4e. In other words, the top is made to look larger. The top carries maximum voltage to provide the electrostatic field whereas the bottom section carries maximum current to provide the magnetic field. As well as top whip the loading coil can be placed below any other form of top of small dimension.

The method has its main application where space is limited and the top is small. It is not as satisfactory as a large capacitive top load. While it does make the current and voltage distribution on the antenna more satisfactory (resulting in a higher radiation resistance), it does add extra losses into the circuit. The tendency to corona is increased.

The inductance of the coil will be much greater to tune the antenna to resonance at the centre than at the base and therefore the coil will be more lossy. Care should be taken not to tune the antenna over resonance or the coil may become very lossy. The best compromise is some centre loading and some base loading. Modern practice appears to be to keep the centre loading coil long and thin to reduce common mode radiation loss. For idealised cases of current distribution, the radiation resistance can be calculated from equations 3, 4 and 6.

The centre loaded whip as well as the helical whip have their main application to portable and mobile, but these applications are not discussed here.

Worked Example

Example 1.—A centre loaded whip has a total height of 35 ft. The distance from the base to the coil is 25 ft. and from the coil to the tip of the whip is 10 ft. Current was measured at the base of the antenna as 1.5 amps. and at the junction between the lower part

and the coil as 1.0 amp. What is the radiation resistance?

From equations 3 and 4

$$F = \frac{(1 + 1.5)}{2} \times 25 + \frac{1 \times 10}{2}$$

$$= 0.69$$

Total electrical height = 0.259.

From equation 6

$$R_a = 98.75 (0.259 \times 0.69)^2$$

$$= 3.17 \text{ ohms.}$$

In the above the current distribution curves were taken as straight lines. If you don't believe that the ammeter can be inserted between the vertical section and the coil, then consider this problem.

Example 2.—In the antenna in Example 1, it was found impossible to insert the ammeter two-thirds of the way up, but it was observed that 38 micro-henries were required at the base to bring the antenna to resonance. What is the radiation resistance? (Solution at some future date if requested.)

METHODS OF FEEDING

When the antenna is series fed, methods of tuning the antenna depend upon the type of load expected. For efficiency it is desirable to use the minimum tuning circuit possible and this is usually a single variable inductance in series with the antenna capacitance. When the antenna is tuned by a series circuit the effective series resistance of the antenna will be presented as a load to the transmitter.

Circuit Fig. 11a is used where the antenna is shorter than a quarter wavelength. Since a short antenna has a low resistance, the tuning circuit of the transmitter must be adequate to handle this. The coupling capacitor of the pi of the final tuning should be large to prevent overcoupling between the two tuned circuits. Overcoupling could result in harmonic radiation and makes tuning difficult. Circuit Fig. 11c is used where the antenna is over resonant—effectively more than a quarter wavelength. Where the antenna is close

to resonant it may be either slightly inductive or capacitive. If the antenna is slightly capacitive, this is simply tuned by only a few turns of inductance, but if the load is slightly inductive a small capacitive reactance is required and hence a very large capacitor. The circuit of Fig. 11b is probably the best to use here. Also, circuit Fig. 11b may be used where no variable inductance is available.

Figs. 11d and 11e are parallel tuned circuits in which the antenna load is effectively in parallel with the tuned circuit. To understand this it is best to consider the effective parallel circuit of the load, Fig. 3. Here the effective parallel resistance is high and the coil behaves as a matching transformer. (It should be realized that there are several ways of looking at these circuits and whether you consider it as a circuit with low series resistance or with a high parallel resistance is a matter of convenience.)

These circuits are particularly applicable where the antenna tuning unit is remote from the transmitter and/or where it is necessary to match into a line. Other arrangements such as pi coupling may also be applicable.

Shunt feeding the lower end of the antenna has some application where the antenna is permanently connected to the ground, Fig. 11f. The antenna is fed with something like a gamma or a half delta match. It is suggested that this method, while satisfactory with a near resonant antenna, could be difficult with a shortened antenna. Large circulating currents would be present in the closed loop of a non resonant antenna which would reduce efficiency and make tuning difficult.

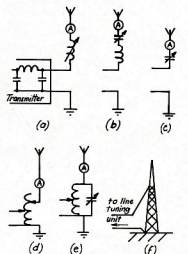


Fig. 11.—Illustrating various methods of feeding and tuning.

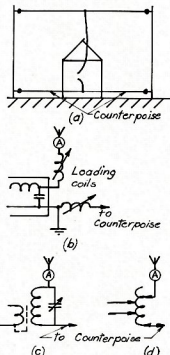


Fig. 12.—Methods of tuning a counterpoise.

EARTHING AND COUNTERPOISING

The most lossy part of a short vertical antenna is the ground. Ground resistance can be reduced by the use of buried earth radials. Unless these are extensive, they are nowhere near as effective as a counterpoise. If we consider the antenna top load as one plate of a capacitor and the ground as another, by using a counterpoise we replace the ground plate with a copper wire.

The counterpoise can be a large web of wire insulated from the ground, but a simple "T" wire directly beneath the top load will produce considerable improvement. If the counterpoise is connected direct to the ground the antenna current will probably drop, indicating a loss rather than an improvement. The counterpoise must be tuned (Figs. 12a and 12b).

A counterpoise can be tuned by a variable inductance or variometer in series with the counterpoise and ground and in this mode it will be parasitic. The loading coils for the aerial and counterpoise must be adjusted alternately to obtain maximum aerial current. When correctly adjusted, the earth current should be small and the aerial current and counterpoise current similar. In practice an ammeter in the ground and counterpoise are unnecessary. Some other methods of tuning are shown in Figs. 12c and 12d which, when tuned correctly, should give zero ground current. These circuits are more difficult to tune than the parasitic counterpoise.

REFERENCES

- Radio Engineers' Handbook, Terman, p. 773.
- Radiotron Designers' Handbook (fourth edition), Reactive component of impedance, p. 903.

☆

Correspondence

Any opinion expressed under this heading is the individual opinion of the writer and does not necessarily coincide with that of the Publishers.

MUNICH OLYMPIC DIPLOMA (M.O.D.)

Editor "A.R." Dear Sir,

I have been asked by Heiner DJ4KU and Maxie DJ4YL, Ballinger, of Munich, West Germany, to pass on information about a certificate called the Munich Olympic Diploma (M.O.D.). The rules for which are as follows:

"All contacts with stations in Munich from January 1, 1970, 0000 GMT to 2000 GMT, the day of the official closing of the Olympic Games 1972 will count for this award. Munich stations are the members of the DOKA C09, C11, C12, C13, C18, C30. Contacts with Munich Amateurs count:

	DL/DJ/DK	Europe	DX
for	2 pts.	4 pts.	6 pts.
per phone	4 pts.	8 pts.	12 pts.

"Class I., 250 points; Class II., 200 points; Class III., 100 points.

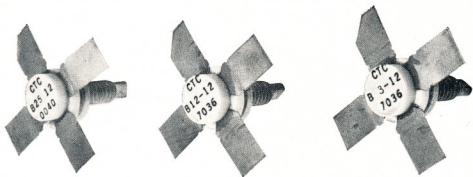
"Mode: cw/phone/mixed. Bands: 160, 80, 40, 20, 15, 10, single band or mixed. The same station may be worked once per band and year. Fees: U.S. \$1.00 or 10 IRC. Send a list of the QSO details certified by two licensed Amateurs to: E. Misera, DJ8ZU, 8 München 13, Keulstr. 6."

If DX operators who are interested in working for this award pass details of their call signs and anticipated operating times, days or dates and bands to me I will pass it on to my contact in Munich.

Incidentally, DJ4KU is blind, and as a consequence obtains a great deal of fun from Amateur Radio.

—S. T. Clark, VK3ASC.

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Amateur Radio, June, 1971

A SOLID STATE F.M. TRANSCEIVER—SOME AFTER-THOUGHTS

By G. L. C. JENKINS,† VK3ZBJ, and H. L. HEPBURN,‡ VK3AFQ

Since the publication of an f.m. receiver design in the March 1971 issue of "A.R." and that for a companion transmitter in the April 1971 issue, some developments have taken place which may be of interest to readers.

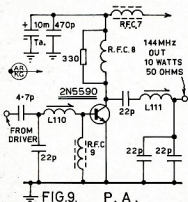
ALTERNATIVE POWER TRANSISTORS

The transmitter design specified the use of a Motorola 2N5589 in the driver section and a Motorola 2N5590 in the p.a.

Varian P/L. of 679 Springvale Road, North Springvale, Vic., 3171 (and 38 Oxley Street, Crows Nest, N.S.W., 2065) suggested that their range of C.T.C. power devices made by the Elmac division of Varian in the U.S.A. might operate well in the circuit. Varian kindly provided a set of devices for trial.

A C.T.C. B3/12 was used in the driver section instead of a 2N5589 and gave somewhat better results. No changes were necessary either to board layout or component values. Used as an output stage on its own, the B3/12 gave well over 2 watts of output power for 70 mW. of drive. It would appear that the B3/12 can be used in the circuit as a direct replacement.

A C.T.C. B12/12 was used in place of the 2N5590 in the p.a. proper, but some component values needed changing. These changes are detailed below. After component optimisation, 15 watts of output were obtained from a 13.6 volt supply rail with 2 watts of drive—a considerable improvement over the 2N5590. At 15 watts out the total current drawn by exciter, driver and p.a. was 2.0 amps.



Referring to Fig. 9, the following component changes are necessary to use the C.T.C. B12/12 in place of the 2N5590:—

- The series input capacitor is increased from 4.7 pF. to 6.8 pF.
- The 22 pF. capacitor between the input end of L110 and earth is reduced to 10 pF.

- L110 is increased from 1½ turns to 2½ turns.
- RFCh is changed to 6 turns of No. 20 tinned copper wire, ⅝" i.d. and ⅝" long.
- L111 is changed to 3½ turns.
- The 330 ohm load resistor across RFCh is not needed.
- The total fixed output capacitance of 44 pF. (2-22 pF. capacitors) to 36 pF. (2-18 pF. capacitors).

The only physical difference between the devices is that the Motorola transistors have a 3/8" diameter case while the C.T.C. transistors have a 5/16" diameter case. Connections are the same.

As a further experiment a C.T.C. B25/12 was driven by the complete transmitter and gave 30 watts of output at 146 MHz. The layout was the same as the existing p.a. but component values were different.

CRYSTAL SPECIFICATIONS

Both transmitter and receiver use crystals in the series mode. With the transmitter especially, it should be noted that the trimming capacitor (and the variations in capacity brought about by the modulating process) are effectively in series with the crystal. When ordering transmitting crystals therefore, the supplier should be advised that they are for use in a series resonant circuit and that they should be calibrated with 25 pF. IN SERIES with the crystal and NOT (as is more normal) in parallel with the crystal.

INCREASING EXCITER D.C. EFFICIENCY

As presented, the current drain of the exciter centres around 70 mA. with perhaps ±10 mA. variation, depending on the spread of characteristics of the devices used.

This d.c. drain can be reduced to a mean value of 45 mA. for a constant r.f. output by some very minor modifications.

Firstly, the oscillator is removed from zener control and given the benefit of full supply voltage. Zener control is retained on the whole modulator section. The effect of this change is to increase the drive from the crystal oscillator. In turn, this increased drive causes the first two MPF121 doublers to saturate and "flat top".

Accordingly, the 47 ohm resistors in the sources of the MPF121 doublers need to be raised to around 330 ohms to bias back the MPF121s into an unsaturated condition. The exact value of source resistors for any individual case must be found by experiment. The simplest indication of arrival at the correct value is when the tuned cir-

cuits associated with each device tune sharply, there is a reduction in total current drain, and the output power remains constant. However the centre value of 330 ohms in each source suggested above will achieve a significant decrease in d.c. power requirements even if the maximum decrease is not achieved.

So far as the transmitter circuit board is concerned physical changes necessary are:—

- Cut the h.t. line between the crystal oscillator and audio sections and bridge the cut with a 1.0K resistor.
- Remove the original 330 ohm zener dropping resistor and replace with an RFC made by threading a single wire through a Neosid F29 slug.
- Transfer the zener diode to a position alongside the 22K modulator trimpot.

TRIMPOTS

The 1.5K and 22K trim pots used are the P.M.D. type made by Plessey/Ducon. They are obtainable from Radio Parts in Melbourne.

The mounting method favoured is to put three circuit board pins in the p.c.b. where the presence of the trim pot is required. The "legs" of the trim pot are bent back at an angle of about 45° and then soldered to the three pins in the board. The legs are bent in such a direction that the adjusting screw of the trim pot will face upward when the trim pot is mounted on the circuit board pins.

TRANSMITTER BASE CHOKES

The "lossy" ferrite rod specified for the base chokes of the driver and p.a. are made by modifying 2½ turn RFCs marketed by the Philips organisation and having the type number 43/2020/36700. As supplied, these chokes consist of 2½ turns of thin tinned copper wire wound through holes in a cylindrical bit of ferrite. The choke is modified so that it consists of two single strands of wire, one strand of wire through each of two holes.

Additional holes are drilled in the printed circuit board about 1/8" away from the choke mounting holes already indicated on the p.c.b. The (four) wire ends of the modified chokes are threaded through the p.c.b., the choke body held hard on the board, and the wires pulled tight before soldering into place.

CIRCUIT BOARD PREPARATION

Several instances have come to the notice of the authors where the printed circuit board, after drilling, has not been cleaned and protected against

(Continued on Page 12)

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‡ 14 Elizabeth Street, East Brighton, Vic., 3187.

THE CLASS C RADIO FREQUENCY AMPLIFIER

LECTURE No. 13

C. A. CULLINAN,* VK3AXU

The class C amplifier is used extensively in radio transmission and a good knowledge of its operation is essential.

By definition this is an amplifier in which the grid bias is appreciably greater than the cut-off value so that the valve plate current is zero when no alternating grid voltage is applied, therefore the plate current in a specific valve flows for appreciably less than one half of each cycle when an alternating grid voltage is applied.

The characteristics of a class C amplifier are high plate circuit efficiency and high power output.

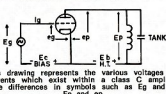
Because the plate current flows only over a portion of each cycle of the exciting grid voltage, the plate current takes the form of pulses and as described in Lecture 10 on Harmonics, the plate output contains considerable distortion.

Class C amplifiers are not used for audio frequency amplification, but when used as radio frequency amplifiers the plate current pulses are converted into sine waves in the amplifier's output circuit if it is properly designed. This action is known as the "fly wheel" effect.

In the discussion which follows, it is assumed that the grid and plate circuits of a class C r.f. amplifier are in resonance and are proportioned so that the radio frequency output of the amplifier will have minimum harmonics.

Also it is assumed that the amplifier has been neutralised if necessary, so that it is stable in operation.

Fig. 1 shows both the various voltage and current relationships which exist within the class C amplifier.



This drawing represents the various voltages and currents which exist within a class C amplifier. Note differences in symbols such as E_g and e_g , E_p and e_p .

The following nomenclature is used:

E_b —d.c. plate voltage.

E_c —grid bias voltage.

E_g —input grid wave (exciting grid voltage).

I_g —peak r.f. grid current.

E_p —voltage across output load circuit (tank circuit).

I_b —d.c. plate current.

I_p —peak r.f. plate current.

e_p —output voltage, plate to cathode.

e_p min.—minimum plate voltage ($E_b - E_p$).

e_g max.—maximum positive grid voltage ($E_g - E_c$).

θ —plate operating angle.

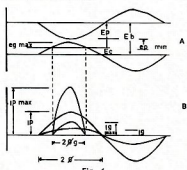
θ_g —grid operating angle.

● Continuing the series of lectures by C. A. Cullinan, VK3AXU, at Broadcast Station 3CS for students studying for a P.M.G. Radio Operator's Certificate.

BIAS

In Fig. 1A E_g is the input voltage, assumed for purposes of simplicity to be a sine wave. This sine wave is impressed on the grid of the valve (between grid and cathode) along with the negative d.c. bias, E_c . This bias will be at least twice the value required for d.c. plate current cut-off. This bias may be obtained from a battery or other constant voltage source, from a grid leak, by the use of a resistor in the cathode of the class C amplifier valve or a combination of these methods.

In a communications continuous wave transmitter it is common to use a constant bias source and to key the transmitter in an earlier stage, thus the class C amplifier valve plate current will be cut-off during key-up conditions of signalling.



In A is shown a graphical representation of the voltages which exist within a class C amplifier. Note that the r.f. plate voltage E_p is 180 degrees out of phase with the grid exciting voltage E_g . In B is shown the relative amplitudes and angles of the flow of currents within a class C amplifier. Particular attention should be made of the plate current pulse which is converted into a sine wave in the "tank" circuit as described in the text.

Theoretically the correct class B bias should be sufficient to reduce the plate current to zero when no excitation is provided at the grid.

Sometimes the keying will be used to add extra bias, beyond the value of the positive grid voltage so that the plate current is reduced to zero. This is known as blocked grid keying. It is frequently used if the oscillator is on the same frequency and may not remain stable in frequency if keyed, i.e. grid excitation is present at all times.

Some types of variable frequency oscillators are very stable and grid-blocked keying of the oscillator may be used. Usually grid blocking voltage is applied to the oscillator and the class

C amplifier in such a way that the oscillator starts a fraction of a second ahead of the class C amplifier and stops just after the amplifier ceases to conduct. This sequence keying is done to prevent the transmission of "chirps" due to minute changes in frequency as the oscillator stops and starts.

When the class C amplifier is used in the plate modulated service for telephony it is usual to employ grid-leak bias, with a small amount of cathode bias as well.

Continuing with Fig. 1A, the a.c. voltage on the plate (E_p) is superimposed on the d.c. plate voltage (E_b). This is 180° out of phase with the grid voltage (E_g).

Grid current flows in the grid circuit as soon as the positive portion of the exciting grid voltage equals the grid bias and plate current then starts to flow.

As the positive portion of the exciting grid voltage continues to rise, so does the plate current until the maximum exciting voltage is reached.

Then this voltage starts to fall and the plate current does likewise to the point where it becomes zero again as the positive exciting voltage reaches the same value as the negative grid bias.

During the rest of the exciting voltage cycle and the beginning of the next, no plate current will flow.

Thus for a sine wave input to the grid the signal in the plate circuit will be in the form of pulses.

This is shown in Fig. 1B which illustrates the relative magnitudes and angles of currents flowing in the circuit. This figure should be studied carefully.

As mentioned earlier, the pulses in the plate circuit will produce a considerable number of harmonics.

To convert these pulses to sine waves the output or "tank" circuit of the amplifier must have a large circulating current (r.f.) and to obtain this it is necessary to have a tank circuit with the proper Q or ratio of k.v.a. to k.w. that is the ratio of volt-amperes in the tank circuit to the d.c. plate power input.

For good harmonic reduction this ratio should be at least 12, although some designers might aim for ratios between 15 and 25.

"FLYWHEEL" ACTION

The "flywheel" action of the tank circuit may be explained as follows:

For ease in understanding this, assume that the output "tank" circuit is in the form of a simple parallel tuned circuit.

When the a.c. exciting grid voltage (E_g) goes positive, plate current (I_p) flows in the "tank" circuit, being superimposed on the d.c. plate current, if the d.c. is fed through the inductance of the "tank".

The a.c. plate current (I_p) flowing in the "tank" circuit produces an r.f. voltage across it, which charges the "tank" condenser, because in our dis-

* 6 Adrian Street, Colac, Vic., 3250.

cussion we are dealing with radio frequencies, not audio frequencies.

Remember, too, from elementary theory that when current flows in a circuit it will produce a voltage across that circuit.

At the moment that the exciting a.c. voltage (Eg) starts to go negative, the condenser of the "tank" circuit starts to discharge towards the plate or anode end of the "tank" circuit to charge the other side of the "tank" condenser through the "tank" inductance.

When the exciting a.c. voltage (Eg) is negative no a.c. plate current (Ip) flows because the valve is cut off, but the "tank" condenser continues to discharge in the opposite direction through the "tank" inductance to charge the other side of the "tank" condenser.

This completes one cycle of the r.f. output and explains how an r.f. pulse in the anode circuit becomes a sine wave in the "tank" circuit.

This explains why it is possible to use a single valve or paralleled valves as an r.f. amplifier in either class C or class B and obtain a sine wave output.

This cannot be done with audio frequencies.

Fig. 2 shows the wave forms of the voltages and currents in a class C amplifier, both unmodulated and modulated. These have been drawn to approximate the conditions which exist in the class C output stage of a 2 kw. broadcast transmitter, but are typical of all class C amplifiers.

RATINGS OF VALVE

In working with class C amplifiers it is desirable to operate within the conditions set down by the valve manufacturer. Any attempt to exceed the published ratings will usually result in short valve life.

Usually two sets of ratings are published—the first known as C.C.S. means

Continuous Commercial Service and is the data used for the design of transmitters which operate more or less continuously. I.C.A.S. is the term used for the second set of ratings and means Intermittent Commercial and Amateur Service. These ratings have been devised on the basis that in I.C.A.S. the users will take a long period of time to obtain the same use or life from a valve that is obtained by a user under the C.C.S. rating and this is the reason that the I.C.A.S. ratings are higher than for C.C.S.

To illustrate this, here is some data taken from an R.C.A. valve data sheet for valve type 833A:—

Service: R.f. power amplifier or oscillator, for class C telephony or class C f.m. telephony. Forced air cooling.

Typical Operation: C.C.S. I.C.A.S.

D.c. plate voltage	4,000	4,000 V.
D.c. grid voltage	-200	-255 V.
Peak r.f. grid voltage	375	415 V.
D.c. plate current	450	500 mA.
Power output		
(approx.)	1,440	1,600 W.

If a class C r.f. amplifier is to be modulated then it is necessary to reduce the ratings from those shown above to prevent damage to the valve.

Service: As a plate modulated r.f. amplifier for class C telephony, the data becomes (forced air cooling):

Typical Operation: C.C.S. I.C.A.S.

D.c. plate voltage	3,000	4,000 V.
D.c. grid voltage	-300	-325 V.
D.c. plate current	415	450 mA.
Power output		
(approx.)	1,000	1,500 W.

The ratings for natural air cooling are considerably reduced from those for forced air cooling.

The above data shows that for C.C.S. class C plate modulated telephony the d.c. plate voltage has been reduced from

4,000 volts to 3,000 volts and the approximate power output drops from 1,500 watts to 1,000 watts. Also note that for frequency modulation the C.C.S. power output is approx. 1,440 watts. This is because for f.m. the carrier power remains constant whereas for a.m. it varies with modulation as explained previously.

Here at 3CS we operate our class C modulated amplifier with four 833A valves in parallel, under C.C.S. ratings.

Examination of the valve life cards, recorded over 15 years, shows that the average life of an 833A valve is 10,000 hours. This includes failures from all causes. The manufacturers guaranteed valve life is 1,500 hours.

In many cases the valves are withdrawn between 10,000 and 12,000 hours use because the harmonic distortion at 3 KHz. to 5 KHz. increases to the allowable limits or because emission of the cathode falls off so that full modulation is not possible on positive peaks (lack of positive peak emission), resulting in asymmetrical modulation.

This falling off of positive peak emission is detected with an amplitude modulation meter and a low distortion audio frequency oscillator, usually long before the modulated amplifier plate current meter shows a reduction of plate current brought about by severe loss of emission.

W.I.A. D.X.C.C.

Listed below are the highest twelve members in each section. Position in the list is determined by the first number shown. The first number represents the participant's total countries less any credits given for deleted countries. The second number shown represents the total D.X.C.C. credits given, including deleted countries. Where totals are the same, listings will be alphabetical by call sign.

Credits for new members and those whose totals have been amended are also shown.

PHONE

VKSMS	318/343	VK4FJ	287/307
VKSRU	317/342	VK2AT	284/288
VK3AH	311/336	VK2APK	281/287
VK6MK	304/324	VK2AAK	274/279
VK4KS	302/317	VK3TL	271/277
VK5AB	297/314	VK4UC	270/270

New Members:

Cert. No.	Call	Total
117	VK3XM	203/201
118	VK3APU	114/114

Amendments:			
VK3ZE	268/271	VK3AMK	230/230
VK4PX	259/260	VK4XJ	158/163

C.W.

VK3QL	303/328	VK3NC	274/300
VK3AHQ	301/315	VK3XB	270/287
VK4FU	299/315	VK3ARK	270/279
VK2AGH	285/286	VK5RU	260/288
VK3YL	281/298	VK4TY	239/272
VK2APK	280/288	VK3TL	235/260

New Member:

Cert. No.	Call	Total
96	VK4KX	178/178

Amendments:			
VK4UC	176/177	VK4XJ	139/145

OPEN

VK5RU	318/343	VK4KS	303/322
VK2AGH	314/334	VK2EO	302/323
VK3VN	310/323	VK3ARK	298/308
VK3SD	306/321	VK3APK	280/288
VK4TY	306/321	VK4EJ	286/323
VK6MK	304/324	VK2SG	294/300

New Member:

Cert. No.	Call	Total
133	VK3APU	116/115

VK4UC	293/294	VK4XJ	194/201
VK4PX	270/273	VK2AXK	122/125

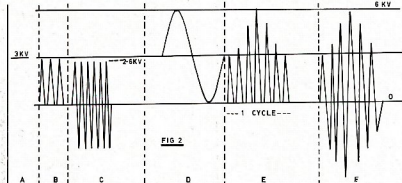


Fig. 2.—Wave forms existing in a class C amplifier in a typical transmitter.

A.—D.c. plate voltage, unmodulated, 3 KV.

B.—R.f. current pulses in the plate circuit, unmodulated (peak 1.0 amp.).

C.—R.f. voltage across the "tank" circuit. The current pulses shown in B have been converted into sine waves in the "tank" circuit because of the "flywheel" action of the "tank", as explained in the text. This drawing is of the voltage that has been produced across the "tank" circuit. By calculation it is 2.5 KV. for this particular transmitter.

D.—Modulated plate voltage. This comprises the audio frequency modulating voltage superimposed on the d.c. plate voltage. That is, above the 3 KV. axis, B plus a.c. modulation voltage, so that peak positive voltage rises to 5 KV. Below the 3 KV. axis, B minus a.c. modulation voltage, so that peak negative voltage drops to zero.

E.—R.f. current pulses in the plate circuit during modulation. The peak positive pulse rises to 2 amps. and on the negative half of the modulating wave the current drops to zero.

F.—The modulated voltage produced across the "tank" circuit because of the "flywheel" action. Because of the small size of the drawings it is not possible to show the r.f. current pulses and resultant sine wave voltages as sine waves, this being the reason that they are drawn in the manner shown.

F.M. TRANSCEIVER

(Continued from Page 9)

oxidation. The effect of these omissions has been to lead to suspect soldered joints and the near impossibility at any later stage to change components, or in any way carry out modifications or repair work.

It is strongly urged therefore that any printed circuit board be cleaned and protected before any soldering work is carried out. This comment does not, of course, apply to boards which have been solder rolled during manufacture.

The simplest way to clean copper circuits boards after drilling is to polish with fine steel wool such as "Jex". Immediately after polishing the clean copper should be given a light coating of clear lacquer. The one recommended is the "metal finish clear" "Spray Pak" put out by Balm Paints under the "Dulux" trade mark.

It is quick drying and (provided a heavy application has not been given) the thin film of lacquer can be soldered through with impunity. Boards treated in this way by the writers are still clean and unoxidised after two years' service and still accept solder as well as the original clean copper.

TUNING UP THE EXCITER

As an alternative to the procedure set out in the April 1971 "A.R." for tuning up the oscillator and doubler stages of the exciter, the following simplified procedure is offered.

It is based on the fact that as the crystal comes into oscillation drive will be applied to the first MPF121 doubler, causing its operating current to rise. As the first doubler starts to put drive into the second doubler, it, in turn, will draw more current. In both doublers there is a by-passed source resistor, the voltage drop across which will rise as drive increases.

Thus the alternative tuning procedure consists simply of putting a high resistance voltmeter or v.t.v.m. on, say, the 5-volt range, across the source resistor of the first MPF121 and adjusting the slugs of L101 and L102 for maximum voltage indication.

The process is repeated with the voltmeter across the source resistor of the second MPF121 doubler, this time adjusting the slugs of L103 and L104 for maximum indication.

It is still necessary to use some form of power meter or r.f. indicator to tune up the MPF121 amplifier.

SIGNAL SOURCE FOR RECEIVER LINE UP

The performance of the receiver is such that to obtain best results the signal level used for final lining up must be very low. Large signals (i.e. 2-3 microvolts or more) cannot successfully be used for final lining up since they cause the whole receiver to saturate.

In the absence of a signal generator with an accurate low level attenuator capable of going down to 0.2/0.3 microvolts, then the simple signal source described by Ron Higginbotham, VK-

3RN in the December 1970 issue of "A.R." is recommended. Several people in the Melbourne area have made up this device using transmit crystals from existing carphones to provide the correct frequency.

If the coupling capacitor between the "High" and "Low" outputs is removed the amount of signal available from the "Low" output terminal appears to be suitable for final lining up of the receiver described.

NEW CALLING, EMERGENCY or SKED-MAKING FREQUENCY 7050 KHz. NEW

Whenever you are in the shack and not operating, keep the receiver running on 7050 KHz.

NEW PROVISIONAL SUNSPOT NUMBERS NEW

FEBRUARY 1971

Dependent on observations at Zurich Observatory and its stations in Locarno and Arosa.

Day	R	Day	R
1	77	15	69
2	78	16	66
3	68	17	82
4	80	18	58
5	53	19	87
6	75	20	91
7	75	21	91
8	50	22	100
9	37	23	87
10	37	24	98
11	52	25	93
12	50	26	69
13	63	27	66
14	56	28	71

Mean equals 71.5

Amended Smoothed Mean for July 1970: 103.3

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AUSTRALIAN 2 METRE F.M. REPEATER DIRECTORY

NEW CALL SIGNS

JANUARY 1971

The Australian development of f.m. repeaters has been along the agreed two-channel principle on Channel 1 (146.1 in and 145.6 out) and Channel 4 (146.4 in and 145.9 out). The simplex operation is on National Channel B (146.0), Channel A (145.854) and Channel C (146.146). The system is based upon a 60 KHz. channel spacing with ± 15 KHz. deviation.

OPERATIONAL REPEATERS

New South Wales:

Sydney—Channel 4, VK2BWI/R1, at Dural. Tx STC base, 40 watts to ground plane at 57 feet. Rx AWA MR20B, ground plane at 57 feet. Separation 250 feet. Coverage approx. 50 miles.

Central West (Orange)—Channel 1, VK2AOA/R1, at Mt. Canoblas. Note: Output is currently on 145.84 but this will be changed to 145.6 later this year. Tx AWA base, 50 watts to ground plane. Rx AWA, ground plane, both 20 feet high. 400 yards separation. Coverage 100 miles.

Victoria

Melbourne—Channel 1, VK3WI/R1, at Carlton. Tx STC 128 base, 50 watts output. Rx is solid state STC 131 with equipment to prevent tx lock-up in event of rx failure. Both antennas are 45' ground planes, 250 feet high with a separation of 600 feet. Coverage approx. 25 m.

Geelong—Channel 4, VK3BGL/R2 located at Gnarwarre. Solid state home-brew equipment. Power output 25 watts. Tx antenna is a folded dipole (temporary) 50 feet up, and receiving is four stacked dipoles 100 feet high. Coverage approx. 60 m.

Gippsland—Channel 4, VK3V1/R3, temporary location at Mt. Bess (near Moe), future permanent location at Mt. Tassie. Solid state I.G.L. equipment, power output 4 to 6 watts. Both antennas are half wave dipoles, receiving 50 feet high, transmitting 35 feet high.

Queensland

Gold Coast—Channel 1, VK4EI/R2, at Mt. Tamborine. Solid state rx, tx home-brew, 25 watts. Antenna 5 x half wave collinear at 40 feet for tx and rx, 250 yards separation. Coverage 50 miles.

South Australia

Adelaide—Channel 4, VK5WI/R1, at Craferas. Tx TCA 1680 solid state 15 watts, rx TCA 1675/777 solid state. Antennas ground plane with small vertical separation. Coverage appears good.

REPEATER APPLICATIONS PENDING

VK2—Newcastle, Mt. Sugarloaf, Ch. 4.
VK6—South Eastern (Albany), Mt. Barker, Ch. 4.
VK7—Northern Tas., Mt. Barrow, Ch. 4.
Hobart, Mt. Wellington, Ch. 1 or Ch. 3.

PLANNING STAGES

VK2—Central Coast, Gosford, Ch. 1.
South Coast, Wollongong, Ch. 1.
Murrumbidgee, Wagga, Ch. 1.
Murray, Albury, Ch. 4.
VK3—North West, Mildura, Ch. 4.
Central—Bendigo, Ch. 4.
VK4—Brisbane, Mt. Cootha, Ch. 4.
VK6—Perth, Tuart Hill, Ch. 4.

CHANNEL ALLOCATIONS FOR POSSIBLE FUTURE DEVELOPMENT

VK1—Canberra, Ch. 4.
VK2—North West, Mt. Kaputar/Narrabri, Ch. 1.
Far West, Cobarr, Ch. 1.
Warrumbungle, Coonabarabran, Ch. 4.
Riverina, Griffith, Ch. 4.
Snowy Mts., Far South Coast, Ch. 1 or 4.
Mid North Coast, Port Macquarie, Ch. 1.
Far North Coast, Grafton, Ch. 4.
VK3—Western, Hamilton/Horsham, Ch. 1.
Northern—Shepparton/Wangaratta, Ch. 1.
VK4—No details known, Ch. 1.
VK5—No further plans at the moment.
VK6—At this stage all possible sites will use Ch. 4, e.g. Narragin/Wagin; Bunbury/Busselton.
VK7—North West, Burnie/Devonport, same channel as finally used by Hobart.

PROJECT AUSTRALIS EXPERIMENTAL REPEATERS

The Australis experimental systems which have the blessing of the P.M.G. Department are designed as a service to enable Amateurs to adjust their equipment in preparation for AO6. It is emphasised that this is not part of the overall repeater plan.

It is possible that similar equipment will be constructed and forwarded to Divisions for use by Amateurs in other States.

One experimental repeater is located at Mt. Dandenong (Vic.). The input frequency is 145.76 MHz and the output frequency is 432.3 MHz. I.G.L. equipment is used. The transmitter output power is 10 watts. Both antennas are quarter wave dipoles about 20 feet high with vertical polarisation in, and, temporarily, vertical polarisation out (this may be horizontal by the time this goes to press).

The other experimental repeater (also I.G.L. equipment) is located at Mt. Bess (near Moe, Vic.). The input frequency is 147.76 MHz and the output frequency is 432.2 MHz. The transmitter output power is 4 to 6 watts. Both antennas are about 15 feet high. The receiver uses a 5/8 co-ax. dipole (vertical polarisation), and the transmitter a 42 element collinear (horizontal polarisation).

VK3ZFJ—J. C. Foster, 26 Avenue Rd., Mosman, 2038.
VK3ZUD—G. O. King, 15 Darnley St., East Sydney, 1507.
VK3ZUP—N. Florio, 6 Pamela Pde., Emu Plains, 2750.
VK3ZUG—P. G. Waiz, 48 Arthur St., Randwick, 2031.
VK3ZUH—J. E. Lukely, 1 Blenheim Pl., Glenfield, 2107.
VK3ZUI—R. C. Eccleston, 2 Valerie St., Mt. Pritchard, 2170.
VK3ZUJ—R. Carr, 275 Main Rd., Toulkley, 2263.
VK3ZUK—D. J. Turner, 82 Amor St., Hornsby, 2077.
VK3ZUL—R. G. Swadling, 3 Grafton St., Lawrence, 2460.
VK3ZUM—G. H. Wilson, 99 River St., Kempsey, 2440.
VK3ZUN—E. S. Turner, 52 Amor St., Hornsby, 2077.
VK3ZUI—E. M. van de Weyer, 101 Francis St., Bondi, 2026.
VK3ZVH/T—W. E. C. Bennett, 5 Hurn St., New Lamb, 2305.
VK3ASV—O. W. Guy, 34 Peter St., Box Hill North, 3182.
VK3BEH—E. E. Russell, 164 Kangaroo Rd., Oakleigh, 3166.
VK3YFC—P. E. Lamb, 28 Panoramic Gr., Glen Waverley, 3150.
VK3YFJ—F. M. Wrobel, 38 Hilton St., Glenroy, 3046.
VK3YFE—S. G. Bushell, 36 Church St., Beaumont, 3193.
VK3YFF—J. C. Buckley, 1/6 Carmichael St., West Footscray, 3012.
VK3YGS—J. W. Tomlinson, 98 Doncaster Rd., North Balwyn, 3104.
VK3ZUR—L. James, 50 Conbermere St., Essendon, 3040.
VK4EI—Central Coast Radio Club, P.O. Box 988, Southport, 4215.
VK4IF—J. F. Miller, 35 Gladstone St., Coorparoo, 4101.
VK4ZF/T—D. G. Hopkins, 11 Stephen St., Morningside, 4170.
VK4ZD—D. J. McWilliam, 2 Rosemary Ave., North Ryde, 1513.
VK4ZGE—G. E. Millward, 4 Mourilyan Rd., Mourilyan, 4886.
VK4ZHI—J. W. Williams, 233 Chapel Hill Rd., Kenmore, 4069.
VK5BW—A. F. Raftery, 22 Princess St., Croydon, 5008.
VK5BU—J. Morris, Flat 20, Hartman Ave., Modbury, 5092.
VK5WI/R1—W.L.A., S.A. Division Inc., Station: Hillcrest, 518.
Craferas, 518.
Post: P.O. Box 1234K, Adelaide, 5001.
VK5WS—W. D. Moulton, 18 Stanley St., Plympton, 5233.
VK5ZJ—C. J. Merry, 26 Davidson Rd., Elizabeth Vale, 5112.
VK5ZJQ—B. D. Norman, Station: Yahl, via Mt. Gambier, 5290; Postal: P.O. Box 177, Mt. Gambier, 5290.
VK6CV—R. W. Walker, 8/278 Scarborough, 3068.
VK6EM—E. S. Harrison, Flat 7, Mitchell Court, 15-17 Mary St., Highgate, 6000.
VK6ND—N. A. Stephen, 19 Leila St., Cannington, 6107.
VK6NW—D. W. Bridge, 109 Sig. Sq., Vincent St., Leederville, 6007.
VK6ZCK—P. Canavan, 55 Grand Promenade, Bayswater, 6053.
VK6ZDN—M. W. Dunning, 46 Holmesdale Rd., West Midland, 6058.
VK6ZJW—T. W. Wadsworth, O.T.C. (A), Carnarvon; Postal: P.O. Box 98, Carnarvon, 6701.
VK7ZBS—G. M. Hanft, 10 Lansdown Cres., West Hobart, 7000.
VK8JH—J. L. Hester, 84 Stanley Cres., Alice Springs, 5750.
VK8JW—R. H. Whellum, Esplanade Hostel, Esplanade, Darwin, 5790.

CANCELLATIONS

VK1JR—J. R. Watson. Not renewed.
VK1ZB—G. W. Fletcher. Not renewed.
VK1ZEB—E. J. Barnes. Not renewed.
VK2AF—P. E. Stuyte. Not renewed.
VK2AIF—M. Burton. Not renewed.
VK2BSP—S. R. Pedemont. Deceased.
VK2ZIS—S. M. Keachle. Not renewed.
VK2ZIE—G. A. Fickett. Not renewed.
VK2ZNG—A. R. Marjoram. Not renewed.
VK2ZST—Sydney Teachers' College Radio Club.
VK3QZ—J. G. Colley. Not renewed.
VK3QV—J. F. Howarth. Deceased.
VK3ABW—M. L. Weeks. Not renewed.
VK3AEP—D. Phillips. Not renewed.
VK3AWD—W. D. Mather. Transferred to Qld.
(Continued on Page 27)

VK-ZL-OCEANIA DX CONTEST, 1970 RESULTS

AUSTRALIA

Phone Section

Call Sign	80	40	20	15	10	Total
AX1GID	—	475	11160	8175	4435	24245
AX1GID	460	110	2315	1340	1065	19040
AX1AOP	—	—	—	2315	1340	3655
AX2KM	425	2625	10390	7220	6040	26700
AX2APK	375	2985	10035	6275	5885	25555
AX2XT	—	11745	4815	3895	20455	—
AX2WC	—	—	1545	4655	2015	12415
AX2EY	—	—	—	—	—	5945
AX2RX	270	—	2575	625	260	3730
AX2AOU	—	—	—	—	—	3700
AX2B	—	—	—	—	—	3420
AX2BDN	—	—	2015	320	570	2895
AX2BNK	565	—	2315	—	—	2770
AX2ABH	—	—	—	—	—	1485
AX2ABC	—	—	1495	—	—	575
AX2UJ	575	—	—	—	—	575
AX3KM	—	11645	2875	2370	16790	—
AX3QV	445	—	3560	—	6405	10410
AX3ASU	—	—	8280	—	9390	—
AX3KS	—	—	3035	—	4785	7820
AX3ASV	575	110	1630	2285	1630	6210
VK3BBA	—	—	5585	—	5585	—
AX3SM	—	—	5985	—	5985	—
AX3ABA	—	—	5155	—	5155	—
AX3ARV	—	—	2535	—	2535	—
VK3BCL	855	—	—	—	—	855
AX4LT	—	—	7270	3185	6010	16465
AX4FT	355	55	1675	5380	12370	—
AX4VX	—	—	—	—	11615	11615
AX4SF	—	—	10720	—	—	10720
VK4EZ	—	—	7285	—	7285	—
AX4LX	210	—	1628	1860	2960	6700
AX4LZ	185	—	3320	1745	525	5785
AX4CJ	—	—	—	—	3800	3800
VK4AN	—	—	1180	—	1500	2680
AX4UA	—	—	800	155	—	955
AX4QA	—	—	—	—	—	—

Call Sign	80	40	20	15	10	Total
AX5WP	—	—	4105	5030	5275	14410
AX5FO	480	495	6075	2735	2320	12105
AX5ZZ	—	—	5650	—	—	5650
AX5ZAC	—	—	1255	75	—	1330
AX6CT	185	2415	5545	3660	3940	13440
AX6RU	335	215	4020	2985	1820	15815
AX6HD	—	—	—	—	13625	13625
AX6LX	—	—	3330	2215	6390	11115
AX7GK	245	805	11340	6480	4275	23145
AX7JV	—	1500	—	—	—	1500
AX8AZ	—	—	1590	985	635	3210
AX9GN	—	355	10405	6915	7665	25340
AX9JL	—	—	2415	115	765	3295
AX9KL	—	—	1860	1985	805	3650
AX9KS	—	—	6130	—	—	6130

C.w. Section

Call Sign	80	40	20	15	10	Total
AX2APK	395	1815	9415	6290	3090	30945
AX2QW	1580	8180	2460	2850	1540	15400
AX2GR	210	900	8355	1525	2335	13585
AX3VN	935	1985	2840	3715	1060	10535
VK3QJ	—	—	—	—	4555	4555
AX2RA	—	—	2625	245	—	3170
AX2BMB	—	—	2240	850	190	2480
AX3VJ	—	—	780	—	—	780
AX2ABC	—	—	620	—	—	620
AX3OP	—	1935	6110	4415	—	12460
AX3AXK	—	—	—	9240	—	9240
AX3APN	—	1140	1960	6495	—	9595
AX3XB	810	—	—	—	5605	6415
VK3MR	—	5550	—	—	—	5550
AX3MJ	—	—	4655	—	—	4655
AX3ASV	—	—	4195	—	—	4195
AX3ABA	—	—	—	2285	—	2285
AX3RJ	—	—	—	—	515	515

Call Sign	80	40	20	15	10	Total
AX4VX	—	—	8915	—	—	8915
AX4UA	—	—	4175	210	—	6305
VK4EZ	—	—	3320	—	—	3320
VK4CX	—	1260	2410	1160	395	5225
AX4CJ	—	—	—	—	4995	4995
AX5FO	—	860	8285	3450	—	12595
AX5FH	615	1790	7565	—	—	9940
AX5FLX	—	—	4865	1985	780	7630
AX5BS	100	—	545	610	285	1840

Call Sign	80	40	20	15	10	Total
AX6HD	—	1370	3415	10115	6405	28125
AX6FL	—	110	110	3330	2585	5715
AX7GK	—	1380	2030	8575	4875	19755
AX8HA	—	—	1940	1560	315	6675
AX9GN	—	—	—	—	9950	9950
VK9XI	—	—	5320	3310	345	5995

VK S.w.I. Section

Call Sign	Phone	C.w.	Total
P. Vernon, L2258	10330	4500	14830
K. Nod, L2949	—	—	8388
R. Ferguson	410	—	410
R. Tremayne, L3286	12285	8510	20795
E. Trebilcock, L3942	—	—	4310
K. Cunningham, L4104	5370	—	5370
P. Drew, L6021	8195	—	8195
R. Mutton (VK7I)	16330	—	16330
R. Everett, L7043	10570	—	10570

NEW ZEALAND

Phone Section

Call Sign	80	40	20	15	10	Total
ZM1AKY	—	385	4170	8190	5150	17895
ZL1AGO	—	1350	3505	7935	2865	13330
(includes 100 pts. on 160 mcs)	—	—	—	—	—	15885
ZM1AIZ	580	705	5290	2855	2700	12130
ZM1AIF	320	—	2505	8715	—	11740
ZM1AAS	—	—	10630	—	—	10630
ZM1AVO	—	—	8425	—	—	8425
ZM1AMM	—	—	4270	1410	—	5680
ZM1ARO	—	—	1740	—	2650	4390
ZM1ACW	—	3970	—	—	—	3970
ZM1TB	—	—	1305	825	2130	4260
ZM2AVY	—	—	9425	1320	—	10745
ZM2QK	—	—	6296	1315	—	7611
ZM2MC	—	—	6060	—	—	6060
ZM2BXC	—	—	6090	—	—	6090
ZM2AWH	1860	—	—	—	—	1860
ZM3US	—	—	7670	375	—	8045
ZL1JG	—	—	4695	—	—	4695
ZM4FX	540	—	7975	610	3200	17855
ZM4DS	505	—	8780	5270	—	14055
ZL4NH	—	—	8425	—	—	8425
ZL4MY	625	—	2225	—	—	2850

C.w. Section

Call Sign	80	40	20	15	10	Total
ZM1HV	100	220	5775	5515	2245	13255
ZM1AMO	—	—	11265	—	—	11265
ZL1DY	—	—	10715	—	—	10715
ZL1JN	55	1815	3435	1090	1050	6545
ZM1AIZ	210	1700	3790	3080	1755	10715
ZM1GX	—	—	2580	1895	3930	8405
ZM1AMM	275	630	5415	2010	—	8460
ZM1IL	—	—	6185	3610	8190	14605
ZM1AF	195	160	3205	675	1335	6020
ZM1BDN	—	—	5585	—	—	5585
ZM1B	—	—	1325	—	—	1325
ZM1BHQ	1090	—	—	—	—	1090
ZL2BCO	—	3085	7585	2710	—	13380
ZL1AJ	—	—	3965	6145	—	10110
ZM2CD	—	—	5235	1335	—	6570
ZM2AH	—	—	1485	1335	—	2820
ZM2WH	950	—	1485	1335	—	2820
ZM3US	—	—	3725	—	—	3725
ZM4A	155	—	8725	—	—	8880
ZM4GA	—	—	6840	—	—	6840
ZM4BO	—	2695	—	—	—	2695
ZM4AT	—	—	4950	—	—	4950

OVERSEAS

Phone Section

Call Sign	Phone	C.w.	Total
DUIFH	48057	YB1HM	700
KHGMPP	36680	YB1CH/KG6	663
KH6J	31400	FKBAH	660
KR6JX	15530	—	—
DL1LN	231	OH1LU	7
DL1G	10818	SMOCS	8
DL1LK	9604	ONSMG	3708
DL1AA	7130	OTKMB	742
DL1PC	5920	OZAPQ	550
DL1UT	1501	PAQ1B	210
DM2AUF	1582	PA0DEC	234
DL1YF	155	PA0JML	178
E3APF	1104	SMOCS	425
E4AKG	192	SMOCER	2940
E4EBN	168	SM1ANT	2126
E4JCW	32	SM0BYG	1458
FR1B	2550	SM0CWK	2210
GP1HO	1980	SM0MC	928
GP1CN	1458	SM1BUS	660
HA1B	91	SM0JN	45
HA3MB	30	SM1AB	238
HB9AA	3366	SM1JVE	196
HB9UD	1040	SP4BDE	1260
IL1AA	5684	—	5684
IL1AMU	1500	SP5CKM	1400
IL1AT	1040	SP1HR	108
IL1AJ	803	SP1AG	803
LA1OI	780	SP1BIX	780
LA1QK	528	SP1BLF	528
LZ1KAA	144	SP1CTN	144
OH1HR	352	SP1KR	2
OH2FS	30	—	—

Asia (excluding Japan)

Call Sign	Phone	C.w.	Total
EP2BQ	5488	OD8BA	24
EP2D	50	ZC4MT	812
MF4BHL	4590	—	—

Japan

Call Sign	Phone	C.w.	Total
JAGADT	685	J43AAW	2408
JAHXHX	442	J43JTH	2185
JABIAM	306	J43BRB	1139
JABECP	30	J43PD	1014
JABOAT	2631	J43BZT	835
JABHVS	2912	J43NDU	792
JABJND	2587	J43JLS	405
JABJUT	1846	J43PL	340
JABKRU	1630	J43BLO	1630
JABHTR	1484	J43XW	5180
JABHNF	1300	J43PM	3588
JABVJR	988	J43BEX	2793
JABHIX	968	J43PHE	1632
JABIAS	420	J43PDD	432
JABHMR	330	J43DDM	184
JABOZ	800	J43Z	80
JABIEU	147	J43U	2976
JABOQR/5	147	J43OQR/5	1120
JABHICW	90	J43HICW	500
JABHJN	27	J43AD	16000
JABOYB	18	J43BSM	1023
JABHJN	8015	J43BY	220
JABHJN	5082	J43HJN	970
JABHJN	1612	J43MA	1193
JABHJN	913	J43KR	1152
JABHJN	578	J43AR	1804
JABHJN	850	J43ARA	8874
JABHJN	828	J43EVL	670
JABHJN	180	J43DVT	217
JABHJN	182	J43AR	1804
JABHJN	55	J43YBA	17262

North and South America

North and South America			
W10KG	3128	K4AQS	1378
K1VTV	1666	WB1DT	168
W2FCR	8602	W0GXN	10471
W2EJR	1125	W0ZKO	1552
W2FNF	1666	W4DEGP	36
W3TLN	15853	W4ZLN	57
W4SHGV	217	HP1JC	2184
W4KE	176	HP1AC	120
W4MGC	136	KZBN	78
W4WSP	504	L4UCO	480
W4WRY	228	O4RV	3612
K4OVN	62	P1NJR	5873
W4WVW	937	W4PAC	904
W4SALB	1300	PY4KL	136
W4SUT	968	PY4AK	320
W4TCB	17	P2GLH	1004
W5RSZ	96	V6VEVY	1686
W4SEPQ	21800	V6GCO	5690
K6SVL	10260	VE1TG	248
K4SEPZ	1666	VE2N	124
W6DGH	5952	V6STO	2334
VE2BNE W6	2440	VE1AH	1132
W6ASTT	7330	X6LLS	7030
W6BJOD	7462	YV4IG	6530
W6RQZ	120	YV1YC	4692
W4BQY	2784		

C.w. Section—Europe (continued)

DM4EL	88	OK2QX	2058
DM2ATL	60	OK1ASJ	30
DM3BE	32	OK1BPE	30
P8TC	1972	OK1BPE	27
P8YV	1020	OK4XG	1552
G8RP	2424	OZ1W	748
OK1CPS	1312	OZ4F7	132
G6XL	1332	OZ3PO	132
GDCD	828	OZ4HW	40
ZUYW	296	PA0JB	428
LA10A	91	PA0VB	216
LA6U	84	PA0BRA	108
LA8CE	70	SM7ANB	2780
LZ2DC	1328	SM7CKX	2488
LZ1KW	48	SM0BYG	1860
LZ2RF	32	SM1EXE	1404
OK1CPS	1312	OZ4F7	132
OH3SE	2775	SM3BUS	304
OH3TY	1008	SP3DQ	1840
OH3R1	608	SP4RY	910
OH3MK	243	SP4Q	126
OH3NW	140	SP4HR	108
OH3XK	40	SP4FL	2
OH3U	12	SP4EBL	1628
OK2RZ	6120	YU4BYZ	200
OK2BOB	3410	YU1SF	4

Japan

JA0JH	367	JA2WK	616
JA0JE	360	JA2EV	610
JA0AC	144	JA2EY	9
JA0PL	1075	JA2Z	616
JA1WI	5216	JA3HT	2425
JA1SR	4620	JA3AAW	1476
JA1KG	3952	JA3MA	208
JA1PB	120	JA3CS	120
JA1KR	2325	JA4X	7409
JA1AF	2236	JA4BX	4202
JA1LH	290	JA4DD	1312
JA1RE	328	JA5MG	1195
JA1PF	784	JA4AQR/S	620
JA1VYK	78	JA5D	88
JA1M	390	JA1T	3880
JA1Z	649	JA1TJ	1700
JA1UC	340	JA1FJ	1340
JA1NM	320	JA1XOY	1102
JA1CA	144	JA1TJ	1102
JA1WC	126	JA1YFA	84
JA1GQZ	80	JA1A	1918
JA1AS	140	JA1GR	216
JA1HC	30	JA8D	150
JA1UT	60	JA8BT	10
JA1H	2300	JA8G	160
JA1ZY	1748	JA9YA	10506
JA2DA	1551	JA9BKU	1062
JA3CP	1067	JA9BN	368

North and South America

WA0KDI	4698	W0RGG	15345
WA0H	376	K6QZ	10440
WA0EPG	370	K6EKR	7320
WA0DS/0	154	W6DGR	6480
W1E2D	12344	W6T2D	6150
W1PL	6658	K6AIV	2464
W1E2D	912	W6CJM	1120
W1SWX	40	W6KHS	720
W1EML	10158	K6MHG/6	546
W1LW	3304	W1E5Q	70
W1VW	3192	W1TR	17820
W1HL	880	W1HIN	10600
W1ZLDX	144	W1SQWN	2000
W1E	746	W1EAC	1000
W1NU	1508	K7JNW	520
W1AZD	3240	PT7BR	72
W1E2D	912	W1E5Q	70
W1SWX	40	W1E5Q	70
W1EML	10158	K6MHG/6	546
W1LW	3304	W1E5Q	70
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W1ZLDX	144	W1SQWN	2000
W1E	746	W1EAC	1000
W1NU	1508	K7JNW	520
W1AZD	3240	PT7BR	72
W1E2D	912	W1E5Q	70
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W1E	746	W1EAC	1000
W1NU	1508	K7JNW	520
W1AZD	3240	PT7BR	72
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W1SWX	40	W1E5Q	70
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W1AZD	3240	PT7BR	72
W1E2D	912	W1E5Q	70
W1SWX	40	W1E5Q	70
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W1ZLDX	144	W1SQWN	2000
W1E	746	W1EAC	1000
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W1ZLDX	144	W1SQWN	2000
W1E	746	W1EAC	1000
W1NU	1508	K7JNW	520
W1AZD	3240	PT7BR	72
W1E2D	912	W1E5Q	70
W1SWX	40	W1E5Q	70
W1EML	10158	K6MHG/6	546
W1LW	3304	W1E5Q	70
W1VW	3192	W1TR	17820
W1HL	880	W1HIN	10600
W1ZLDX	144	W1SQWN	2000
W1E	746	W1EAC	1000
W1NU	1508	K7JNW	520
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AUSTRALIS BALLOON FLIGHTS—A PRELIMINARY REPORT

By RICHARD TONKIN*

This article represents a preliminary report on the results of the recent flights of the Australis translator system on balloon packages. Because all of the tapes and other data from the flights has not yet been analysed, a complete list of the Amateurs who worked through the package, and further details on the results of the flights will be held over until the next issue of "A.R."

The main reasons for conducting the balloon flights with the Australis translator were to demonstrate its operation over relatively long distances and to experiment with antenna systems which could be used on any future flights. The translator used was a prototype of one of the four channels which, if all goes well, will fly on the A-O-B satellite next year. The translator was built by Les Jenkins, VK3ZBJ. Its input was 146.00 MHz. (Channel B, f.m.), with the output on 432.30 MHz. The power output was approximately 500 milliwatts. Prior to the balloon flights, the translator had been operated for several weeks on top of Mt. Dandenong, near Melbourne, and a considerable amount of interest was shown by Amateurs in this test.

Permission was obtained from the Department of Supply to fly the translator as a "piggyback" experiment on the March-April series of scientific research balloon flights from Mildura, about 350 miles north-west of Melbourne. The balloon series, called HIBAL, consisted, so far as the Australis translator package was concerned, of four flights, to 70,000 (70K), 90,000 (90K), 105,000 (105K) and 120,000 (120K) feet.

The balloons are several hundred feet high when launched and they gradually assume a spherical shape as they rise into the upper atmosphere. The payload, or gondola, consists of a tubular steel frame inside which the equipment is located. The gondola is about the size of a small car, and weighs an average of about 500 lbs.—so HIBAL is no mean balloon!

After launch from Mildura airport, the helium-filled balloon rises at a rate of about 1,000 feet per minute until it reaches its float altitude. The length of time that the balloon and its payload float depends on the type of experiment being flown, but two to three hours was the average float time for the four flights on which the Australis package was hitching a ride. At the end of the float period, a radio command transmitted to the gondola from the HIBAL control station at Mildura airport separates the balloon from the gondola. As the gondola drops into the denser layers of the atmosphere, a parachute opens and lowers the payload to the ground. A chase aircraft follows the gondola's descent and radios its landing position to HIBAL Land-Rovers which travel to the landing site and recover the payload.

George Long, VK3YDB, who prepared the translator for the flights, and I travelled to Mildura before the first flight to test the translator with the HIBAL packages, settle the final flight details with the HIBAL personnel and meet the Amateurs at Mildura who had previously offered their help with the flights. The Amateurs who assisted the project at Mildura included Mike VK-3CCX, who was a real tower of strength and who, being a member of the HIBAL crew, was able to give invaluable technical assistance on the four flights; Noel VK3AGF, who did a fine job in communicating with the anxious project members in Melbourne; Graham VK-3YEJ, Joan VK3YEK and her OM, Ray VK3ZBN. Without the seemingly tireless help of these people, it would not have been possible to fly the Australis translator on the HIBAL flights.

The four flights were launched at about dawn on 23rd March (70K), 25th March (105K), 2nd April (90K) and 5th April (120K). All flights rose to their planned altitudes and the translator worked well on the four trips it took into the stratosphere. The same translator unit was used on each flight and it was recovered undamaged after each flight. Before the flights began, it had been calculated that the Mildura launch site and the planned float altitudes would allow Amateurs in Adelaide and Melbourne (and points in between) to maintain contact during the ascent and float phases of the flights. We were a little more optimistic about the 120K flight and we hoped, because of the greater altitude it would reach, that we may be able to get signals into it from further afield than Melbourne.

In the event, Adelaide-Melbourne (and vice versa) QSOs were achieved on all four flights. The copy varied from unreadable to numerous dBs over S9, depending on the power that the transmitting station was putting into the translator, how many people were trying to get into it at the same time, and the orientation of the antenna system on the gondola. The 2 metre receive aerial was a vertical ground plane and the 432 MHz. transmitting antenna was an omni-directional turnstile. For the 70K and 120K flights, the antenna system was mounted on the top of the HIBAL gondola and on the 105K and 90K flights it was located on the bottom of the gondola. These were the two most convenient positions to put the antennas, having regard to the need to keep the Australis aerials away from the HIBAL equipment and taking into account the shadowing effect which the gondola frame and the HIBAL equipments had on the Australis antenna radiation patterns.

The results from the four flights was very interesting and it appears, from initial data that have been looked at, as though the top-located antennas (70K and 120K flights) operated better than the bottom-mounted ones (105K

and 90K flights), at least so far as Melbourne Amateurs were concerned. It is possible that atmospheric temperature inversions played a part in some of the long signal fades which occurred during the flights. It is hoped that a more complete report on these aspects of the flights can be included in a later issue of "A.R."

The following is a preliminary list of Amateurs who worked through one or more of the translator flights. As mentioned above, this is not a complete list and represents only the call signs heard on some of the tapes of the flights. The complete list and more details of each flight will be in July "A.R."

VKs 5ZDR, 6NZ, 5QZ, 5ZK.

VKs 3ZCE, 3YFI, 3FW, 3YBO, 3ZBJ, 3YDB, 3AGF, 3YEJ, 3ASV, 3AKC.

VKs 1VP and 2ZHM.

There are probably at least another six VK5 calls who worked through the translator and a couple of other VK3 ones as well. It would be a great help if the people who worked through it would drop me a line and give me the date, power output used, antenna used, stations heard, etc. As is usual with projects of this kind, we tend to be enthusiastic about it while the action is there, but a little remiss when it comes to looking back through the log book and putting pen to paper. An appeal on the VK3 and VK5 Divisional broadcasts yielded only one written report, so please sharpen up the pencils and send in your report, plus any comments, good or bad, that you have about the flights. After all, the Amateurs of Australia, through the Institute, are paying for the Australis project and they should be making the best use of the balloon flights and of the satellite to follow.

It was particularly pleasing, on the 120K flight, to hear Eddie VK1VP in Canberra and John VK2ZHM at Cootamundra, coming through the translator. The sort of distances covered in that flight give some idea of the coverage which will be possible with the A-O-B satellite, when VK-JA contacts should become commonplace on v.h.f.

The co-operation given to the Australis balloon project by Mr. John Hillier and his team at the balloon launching station at Mildura deserves special mention. The Australis translator was flown on a space, weight and power-available basis. While it was originally planned that there would be only one translator flight in the March-April series of balloon launchings, George VK3YDB, by going to Mildura and talking with the HIBAL people, was able to arrange that the package flew on four, rather than one, flight. The active assistance given by John Hillier and his team in arranging the flights is greatly appreciated by the W.I.A.-Australis group.

(Continued on Page 27)

*Chairman, Project Australis, 13 Nestan Dr., Ringwood, Vic., 3134.

KEY SECTION

During the 1930s an active element of Institute affairs was a group known as the Key Section. It appears to have dropped into limbo (with so many other things) in the early 40s, and did not re-appear after the war.

The 1971 Federal Convention in Brisbane agreed to revive the Key Section, and the rules for its operation which were accepted were these:—

1. That the Key Section be open to all members who have worked at least 50 different stations by two-way radio contact using A1 or A2 mode. To qualify as a contact significant text should be exchanged, say, 30 words apart from RST; operations during contests are excluded.

2. That the Federal President's Cup, awarded to the Key Section of the W.I.A. in 1930, be revived and mounted and awarded annually with inscription to the member of the section who claims the greatest number of contacts using A1 or A2 mode in that year. No member may hold the cup for more than two successive years.

3. That the W.I.A. make available to overseas Amateurs a certificate or other token for working 20 or more members of the Key Section of the W.I.A.

4. That the W.I.A., through its Key Section, make available certificates of proficiency to members of the Section for successfully receiving and sending using A1 or A2 mode at speeds of 15, 20, 25 and 30 plus words per minute.

5. That the Federal Contest Manager be approached to alter the rules of W.I.A. contests to remove the bias against the use of A1 in contests (because of the lower scoring rates which can be achieved using this mode under contest conditions in Australia), such as by offering a multiplying factor for all contacts using A1 or A2 mode.

6. That every method be used to introduce more A1 or A2 to the v.h.f. bands even to the extent of making operation of v.h.f. part of the requirement for some of the awards associated with the Key Section.

7. That the Key Section be managed by a group consisting of an officer appointed by the Federal Executive and a nominee of each Divisional Council.

8. The nominee of Federal Executive will act as nominal head of the group and report the activities of the Key Section to the Federal Council.

9. The Divisional nominees will be appointed by Divisional Councils and will be known as Divisional Co-ordinators. Appointment will normally be for a period of three years.

10. In the event of a Divisional Co-ordinator resigning, or being replaced as nominee by the Divisional Council, a new nominee will be appointed by the Divisional Council, the tenure dating from the time of the new appointment.

11. The Divisional Co-ordinator may call upon the services of not more than three other persons, whose appointment must be ratified by the Divisional Council, to assist him.

The Federal Executive have appointed Deane Blackman, VK3TX, as Key Section Manager. The appointment of Divisional Co-ordinators, which is the next task in setting up the Section, is in hand.

ANNOUNCING A SPECIAL CALL AND PREFIX

KC0KC will be heard on all bands for the period 1st July, 1971, through to 5th July, 1971. Members of the Mobile Amateur Radio Awards Club Inc. (M.A.R.A.C.) and the Independent County Hunters' Nets meeting in Kansas City through these dates will man the station around the clock.

KC0KC will be on 10, 15 and 20 metres, beginning when the band opens in Kansas City around 1300 GMT until the band closes late in the evening. Activity on 40 and 80 metres will probably begin around 2200 hours GMT until 1300 GMT the following day. However activity will generally be on any band at any time that band is open.

Activity is planned around the following frequencies:—

	CW	Phone(1)	Phone(2)
80 Metres	3550	3680	3910
40 "	7050	7205	7260
20 "	14050	14205	14285
15 "	21050	21280	21360
10 "	29050	29600	

Notes: (1) Several times each hour operator will announce and listen 5 or 10 KHz. below the bottom of the U.S. phone band for DX stations.

(2) If "pile-ups" develop, operator may listen off his transmitting frequency.

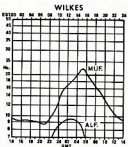
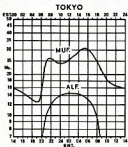
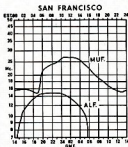
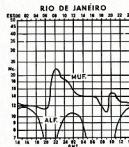
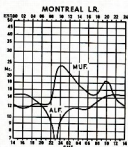
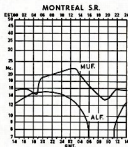
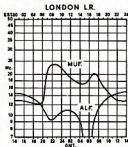
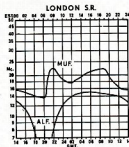
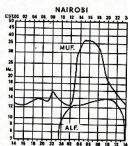
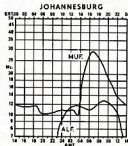
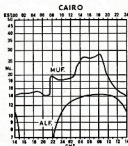
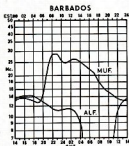
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May Tak to You About the 35th Federal Convention in Brisbane

In last month's "A.R." the "Wind of Change" was mentioned as if it had been something sudden. It is and yet it isn't. Zephyr breezes have blown for some little while. They have now increased to the point where their influence is doing much to improve the exchange of information in an efficient way at a meeting such as the Convention. Every Divisional Councillor and the many observers at the Convention all commented on this. Your Federal President is largely responsible for this. His overseas trips helped, of course, enormously. The main objective for all of us is communication — effective communication. If this can be achieved more positively with less formality, so much the better. The pendulum could swing too far the other way. This is recognised. But we are dealing with persons, not faceless monsters or remote bodies out of reach and out of touch.

Which brings me back to people. Recognition of problems and genuine attempts to resolve them. This is what the Convention is all about. This is what the Delegates dealt with. Year problems year troubles. I.T.U. and I.A.R.U. seem remote. Not your problems you might say. How wrong could you be? You want W.I.A. to be there to help you in so many ways. In the beginning to help you to learn the fundamentals of electronics, to absorb and use the Morse Code, and to put you in touch with cheap gear and components. Later on the emphasis shifts as you yourself develop expanding interests. You are hedged about by Regulations, far too many of them you may say. In 1910 the W.I.A. began. Not only for social contact. Not only to present a united front. But also the sharing of benefits which only a larger group can command. No, I will not enlarge on this here except to say that the W.I.A. interest in I.A.R.U. is not misplaced. Without the united front—worldwide—we would definitely not possess the funds we have today. Pressures by commerce, by governmental agencies and by many other services would have seen to that.

So, at the Convention, I.A.R.U. and I.T.U. matters received much attention because Michael Owen, VK3CZ, and Peter Williams, VK3IZ, had returned a few days beforehand from the I.A.R.U. Region III, Association Conference in Tokyo and the I.T.U. Space Conference is scheduled for July in Geneva. Yes, plans had been laid. Keep your fingers crossed; we might keep what we have. We could even hope to gain a little ground. For I.A.R.U. affairs, David Rankin, VK3QV, was appointed to be our Liaison Officer.

Equally, at this Convention, the financial side of W.I.A.'s affairs got a very good airing. The theme was how to do more at less cost. Facts of life have to be faced however. There was absolutely no question of how to squeeze more money out of members. In fact the contrary applied. Can we do anything more for members within our budget and, if so, what and how? As a newcomer to the Australian scene I was impressed by the massive amount of thought devoted to financial matters. I assure you it was not put on for my benefit. I am too old a hand to be hoodwinked into a belief that this was mere window-dressing.

The proposed computerisation (horrible word!) programme took two full pages of my notes. It stands to reason that, if the thing is done properly, savings can accrue. The most fantastic depth of detail unfolded before Delegates' eyes. Even down to such minutiae as how to preserve the confidential nature of information to be sought from members. How to get essential data and the practical steps required to process it were all covered as well as the relative importance of the end result. The computer can churn out, in seconds, any collection of detail which may be required. Not only prints-out of names, call signs and addresses for the club books, full magazine wrappers and unpleen other needs—transient and permanent—subscriptions and their apportionment, but, furthermore, bulk statistics of one kind or another which Federal Executive must have in their endeavours to convince disbelieving authorities of the correctness of their submissions. So, if you have to send your subscription to Melbourne next year or, if you are asked for any details you think may be important, don't worry. The whole thing is under the most rigid Divisional control. The Federal boys will not run away with the lot or misuse it.

Various technical affairs also took up a lot of time. Interference against us and by us and how best to achieve satisfactory results. After all we pay fees equivalent to others but receive different treatment. The U.S.A. phone operators petitioning F.C.C. for a further 50 KHz. downward of band allocations and how we can most effectively display our opposition.

Project Australis and the dearth of details for you received much comment on how to put this right. The back-room group are doing a splendid job all right, but for goodness' sake let us. Our money is involved apart from anything else. So, a plan was devised and John Battrock, VK3OB, is the corner-stone. Now the V.H.f. Groups in Divisions will have a chance to play with the flight-tested package. Dr. Denise Blackman's proposed Key Section got off the ground. Traffic nets regularisation (a.s.b. vox), operators' identification "at the beginning and end" of transmissions—what is a "transmission", how long, break-in—7050 KHz. was designated as a calling frequency as, for example, calling for aid on safari or using it for sled-making and then QSY'ing elsewhere—people could leave their receivers running on this frequency—and so on. Space does not allow me to go into details I fear.

"So You Want to Become an Amateur" booklet is now in print and a very good one it is too. The only error detected so far is the fee payable when applying to sit for the exam; should, of course, be £2.00 but there are rumblings about raising it. The new Call Book should be out by the time you read this. Much criticism about the delay, which, incidentally, was not our fault. How to deal with "A.R." and Divisional Bulletins—how can we economise without lowering standards?

Is that all? Do not be deluded. The discussions on the "Novice" licensing report received only a week beforehand by the way) from Mr. Rex Black's (VK2YA) Committee got through seven pages of my notes. What

do you mean by "Novice" licensing? Like the JAs on 15 metres? No, but definitely no. The report was too good to set it on one side but much more thought and discussion is required before we can go further. Delegates have it. Why not ask about it? As one Delegate aptly remarked, "It's a large thing with few knobs to hold on to." General organisation and the efficient administration of W.I.A. affairs received attention in the light of the impending change-over to the new Federal Constitution after the W.I.A. Company Memorandum and Articles of Association have been signed, sealed and delivered. All this was, of course, tied into with the annual reception of A.R.'s policy, and the role of the new Secretary-Manager.

Those who were in the 23 years of age group in 1910 would now be in their eighties. With the years, most of the pioneers will be passing on. The Convention again devoted time to ways and means to accumulate and preserve items of historical interest. The onus has been placed on Divisions to examine this aspect, possibly by seeking the aid of local libraries and museums. Let us gather together everything we can before it is too late.

Another item was the change-over of the Federal Contest Committee from VK3K to VK4. What a magnificent job they did on this over the past six years and we look forward to another good period, especially as we believe Peter Brown, VK4JF, is much up to the job. Symptomatic of the times, by the way, were the very reduced numbers of agenda items about contests and awards rules. A good thing this, so please don't brew up a load of new alterations! Let the people in VK4 get the best of the thing. Geoff Wilson, VK3IAM, naturally got a commendation on Federal Awards, especially for his excellent handling of the Cook Bi-Centenary Award. Ken Pincot, VK3LC, was commended on his work of running the Publications Department which will henceforth land up on my table.

I know I have had to leave out a lot, e.g. repeaters and beacons, badges, publications, policies, submissions about multiple-choice examination papers and operating procedures, etc. Don Wainman, VK3JF, will vouch for this. He sat in as an "observer" for the VK5 Delegate. This was another new departure. The local Division provided "observers" for the far-flung Delegates and this innovation was much appreciated not only by the Delegates but also by the "observers" themselves. The point is well taken, with innovations and modernisation, that we must keep the best of what we have however.

The venue of the next Convention is to be Melbourne for several valid reasons.

I started off this article about the I.T.U. and I'll end about it also. Tom Clarkson, ZL2AZ, will be attending the big July Convention in Geneva as an observer on our behalf. As somebody said, it would be difficult to find a better qualified observer anywhere. In Region III, which encompasses the whole area roughly from India to the mid-Pacific. The Delegates to this Conference are officials of governments. Amateur Radio is only a small part of the whole and must be content with observers. We've done our part with your government. Have you done your part with your Division?

72, VK3CIP.



Photograph of Federal Executive Delegates at the Brisbane Convention of the W.I.A., held over Easter. Right to left: David H. Rankin, VK3CZ; Peter D. Williams, VK3IZ; Michael Owen, VK3CJ (President); Peter B. Dodd, VK3CIP (Sec. Man.); Ken E. Pincot, VK3AF (Editor "A.R.K").

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Victorian Division
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commences

MONDAY, 16th AUG., 1971
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Adjustment of Output and Loading, SSB Transmitters

HEATHKIT SB-610 MONITORSCOPE AND HEATHKIT HN-31 ANTENNA

It is well known that a cathode ray oscilloscope is a valuable aid in checking the operation of a transmitter. The usual CRO is primarily a general purpose instrument for the laboratory or electronics workshop and is not always convenient to use in the Amateur shack on a permanent monitoring basis. The **Heathkit SB-610 Monitorscope** fills the gap, as it is designed to be connected into a 50-72 ohm antenna feeder line, includes a built-in two-tone audio oscillator, is compact in size, and styled to harmonise with the equipment.

Adjustment of an output pi network of a PA stage requires care in order to obtain the highest possible RF voltage peaks without "flat topping". Some manufacturers give approximate settings of the loading control for each band, which with plate tuning resonance, is intended to assist the operator to reach this objective.

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The SB-610 also has provision for coupling to a receiver to enable visual monitoring of received signals. In addition, the instrument, with its H sweep and V amp., is useful for other CRO testing applications in the Amateur shack. A comprehensive instruction manual describes the various features and installation procedure, and operating instructions include representative screen patterns showing examples of correct and incorrect tuning not only for the SSB mode, but for AM, also keying patterns for CW, RTTY adjustments, etc.

It is recommended that tuning up be carried out with the transmitter output connected to a non-inductive dummy load. The Heathkit HN-31 Antenna is designed for this purpose.

Brief Details

SB-610, applicable over the range 160 to 6 metres, has standard UHF co-ax. sockets for ready connection into co-ax. feed line, 3" mu-metal shielded CRT, power requirement 240 V. AC 50 c/s. Size: 6" h. x 10" w. x 11" d.

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I.A.R.U. REGION 3 ASSOCIATION CONFERENCE, TOYKO, 1971

BACKGROUND TO CONFERENCE

At the Conference of Sydney 1968 at which the Region III. Association was formed, it was decided to give the J.A.R.L. the right of invitation to extend to have it in Tokyo. This was confirmed and preliminary details completed in January 1971.

In collaboration with the Secretariat, J.A.R.L. made arrangements for the Conference to be held at the Fairmont Hotel and the Zenkoyoren Building, Tokyo. The meetings commenced with a preliminary informal one on 15th March with formal sessions on 17th, 18th and 19th March, and a concluding one on 21st March.

LIST OF PARTICIPANTS

I.A.R.U.: W0DX, Mr. R. W. Denniston.
Australia: VK3KI, Mr. M. Owen; VK3VX, Mr. A. G. Fitter.
New Zealand: ZL4PC, Mr. D. A. Lloyd;
ZL2AZ, Mr. T. R. Clarkson.
Philippines: DU1KA, Mr. E. M. Aristores;
DU1BH, Mr. R. B. Nolasco;
Mr. B. P. C. Esquerra; DU1ER, Mr. H. del Rosario; DU1SA, Mr. S. A. del Rosero; DU1WO, Mr. E. Crabe.
India: VU2US, Mr. K. Umrao Singh.
Hong Kong: VS8AI, Mr. G. Flenner; VS8DR, Mr. P. Wight.
Japan: JA1AN, Mr. S. Hara; JA1BK, Mr. K. Mizoguchi; JA1NET, Mr. S. Morimoto;
JA0LA, Mr. K. Kuwazawa.
Secretary: VK3LZ, Mr. P. D. Williams.

ARRANGEMENTS FOR MEETINGS

After the first meeting was opened by the Secretary-General, the head of the J.A.R.L. delegation (Mr. S. Hara, JA1AN, President of J.A.R.L.) welcomed the delegates and gave an oratory Chairman of the Conference. After welcoming the Delegates to Tokyo, he invited nominations for the officers of the Conference. Mr. R. W. Denniston, W0DX, was elected Chairman, and Mr. P. D. Williams, VK3LZ, Secretary. The J.A.R.L. described the arrangements for the conference and the Secretary in the practical work involved.

THE MEMBER SOCIETIES

Credentials were submitted by the Societies qualified according to the Interim Constitution and it was agreed that, in addition to existing membership, the societies of India, Ceylon, Hong Kong would be members and the American Radio Relay League would be a member, in view of the members it has in Region III.

STATUS OF CONFERENCE

In order to clear up some imperfections in the Interim Constitution, the degree of authority of the Conference was discussed, and it being decided that it was competent to do so, several amendments were made in the Interim Constitution, their purpose to affirm that membership in "I.A.R.U." was open to all societies in the Region III. Association. As a result, P.A.R.A. became the member Society to represent the Philippines. So the member societies represented and eligible to vote at the meeting were W.I.A., A.R.R.L., N.Z.A.R.T., P.A.R.A., A.R.S.I., J.A.R.L., H.A.R.T.S. The agenda prepared at the preliminary meeting was approved. Reference is now made to the topics discussed and conclusions reached.

THE CONSTITUTION

After receiving from the Secretary-General on the activities of the last three years, and the financial position, and approving the final statement from the Sydney 1968 meeting, consideration was given to matters concerning the organisation of the Association and these revolved around the preparation of a Constitution to meet all foreign requirements. After prolonged study the principles to be incorporated in a Constitution were agreed. Details are in the Minutes of the new Constitution, salient points being—

1. Conferences held at intervals of three to four years will control the Association. Between Conferences matters requiring the decision by member Societies will be dealt with by post.

2. Each Society will designate a Liaison Officer to be its representative in Association affairs.
3. The inviting Society will be expected to facilitate the efficient and economical running of the Conference, but not to bear the "out-of-pocket" expense that may be entailed. The cost of travel and accommodation for Delegates will be the responsibility of their Society.
4. The management of the Association will be done by four Directors and a Secretary, who will be appointed by the Conference on a personal basis and be responsible to it. Expenses incurred for the Directors and Secretary to carry out the duties will be the responsibility of the Association. This includes attendance at Conferences, at which Directors will participate, but not on behalf of a member Society. Directors and Secretary will be appointed to act until the conclusion of the following Conference.
5. Rules of Procedure for Conferences are to be observed and they form Regulations attached to the Constitution.
6. Subscriptions are to be paid by member Societies, the amount being based on the number of members—the maximum being 15 cents (U.S.) per member with lower figures where there are more members. The minimum subscription to be \$25 per annum.

CURRENT SUBJECTS STUDIED

The I.T.U. World Space Conference—The present situation regarding the approach to the Space Conference was described by W0DX, who as President of I.A.R.U., will be the official observer for the Union at the I.T.U. Space Conference. The status of negotiations with their Administrations was outlined by all representatives present and appreciation of the great importance to Amateur Radio of strong representation at Geneva.

W0DX described how he was enlisting the aid of all resources available in his task and how Region I. and Region II. would be represented in his team. He pointed out the high desirability of Region III. being represented to make his team a truly representative one of world Amateur Radio.

After prolonged study, the Conference decided on the principle that the Association should send a representative and considered the practicability of meeting the high costs involved. It was apparent that some extraordinary means of finding the funds would be needed, and as these were considered to be justified, it was decided to seek credit for the amount needed and to plan its repayment over several years.

Assuming the success of these arrangements for a representative, the person to be nominated by the leader of the team, W0DX, and to be approved by the Directors. This is being done at a Directors' meeting on 19th March and ZL2AZ, Mr. T. R. Clarkson, was appointed.

The 7 MHz. Band.—The need for more spectrum space for the Amateur Service on an exclusive basis was emphasised. This is being pursued. As a general world administrative frequency conference seems to be in the very distant future, the best approach is a "piece meal" one and each Society was urged to try and get agreement by its Administration with a view to getting first national, then regional, and eventually world-wide expansion of the exclusive segment.

A survey of interference on the 7 MHz. band was presented by J.A.R.L. with the result of recent automatic recordings. After discussion of possible methods of meeting the situation, the Conference resolved that all Societies would actively pursue the subject of improving the 7 MHz. band situation.

Development and Encouragement of Amateur Radio Activity in Region III.—Among proposals to encourage activity in the Region a new type of award was suggested. This would recognise the merit of conducting recurrent QSOs in contrast to the brief single ones. This is being studied by several interested Societies.

Publicity and Public Relations.—Societies were urged to try and get Amateur Radio activities brought under notice of the public at large by seeing publicity in the news media. News items such as the holding of the current Conference can be used to introduce influential reports of amateurs and their activities. Societies should make known to others their success in this field.

Election of Directors.—The following were elected to be Directors: JA1BK, VK3KI, ZL2AZ, and W0DX.

Election of Secretary: VK3LZ.

Next Conference.—Hong Kong under auspices of H.A.R.T.S.

Invitations were extended by three Societies who offered to have the next Conference, namely, P.A.R.A., H.A.R.T.S. and A.R.S.I. After full consideration it was decided to accept the invitation of H.A.R.T.S. for it to be held in Hong Kong.

A Final Point.—As indicated in the provisions of the Constitution it is recognised that all expenses for Delegates to attend Conferences should be borne by their Societies. This decision highlights the special indebtedness of all concerned, first to W.I.A. and now to J.A.R.L. for meeting Delegates' accommodation expenses, which action has assured the success of the two Conferences—a most significant factor in the important formative stage of the I.A.R.U. Region III. Association.

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- ★ "CQ" Magazine, \$5.70; Three Years, \$13.50.
- ★ "73" Magazine, \$5.50; Three Years, \$11.50.
- ★ "Ham Radio" Magazine, \$5.50; Three Years, \$11.50.
- ★ N.Z.A.R.T. "Break-In", \$3.00.
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NEW NEW
YOUR I.A.R.U. REGION III. OFFICER
IS DAVID RANKIN, VK3OV
NEW NEW

Amateur Radio, June,

Sub-Editor: ERIC JAMIESON, VKSLP
 Forreston, South Australia, 5233.
 Closing date for copy 30th of month.
 All Times in E.S.T.

AMATEUR BAND BEACONS

VK0	63.544	VK6GH, Antarctica.
VK3	144.000	VK1KJ, Vermilion, S.A.
VK4	144.390	VK4VV, 107m, w. of Brisbane.
VK5	63.030	VK5VF, Mt. Lofy.
VK6	144.800	VK6VF, Mt. Lofy.
	152.095	VK6VF, Tuart Hill, W.A.
	52.800	VK6TS, Carnarvon.
	144.500	VK6VE, Mt. Barker.
	145.010	VK6VF, Tuart Hill, W.A.
	435.000	VK6VF (on by arrangement).
VK7	144.800	VK7VF, Devonport.
VK9	144.600	VK9KJ, Christmas Island.
ZL2	145.200	ZL2VHF, Wellington.
ZL3	145.000	ZL3VHF, Christchurch.
VA	51.965	JA1GY, Japan.
V	50.091	WB6KA, U.S.A.
NK	50.100	HL9W, South Korea.
ZL	50.100	ZK1AA, Cook Island.
KH6	50.101	KH6SO, Hawaii.

The Cook Island beacon is included this month although it has been around for some time. Doug VK6KKE in Darwin reports hearing it on 4th April with signals S4. The Hawaii beacon KH6SO is reported to operate nominally around 50.100, but reports indicate the frequency varies as high as 0.107. Doug has been hearing it with some regularity in Darwin with varying signal strengths, rising to S89 on 25th April at 1315 hours. It has also been heard by Ross VK4RO and David VK4AU. It is a rather frustrating signal, however, as Doug reports that if you hear the beacon and dial 435.010 in Hawaii, after eight rings or so you will hear a tone and then a voice. In this state you can then work yourself? As Doug says, "Just hook your trunk call to KH6 and hear the tone and then the voice. I don't know whether he ever listens on 52 MHz."

Further notes on the Darwin scene are that six more reports have been received before long on 52.390. (This is very pleasing information and further details are awaited.—SLP.) Good signals to Bob CZ2 in many times, plus for Doug VK6VF seems to be a pipeline that way. Seems as though it is double hop F2 at KH6 with CZ1 on the first hop. HL9W in South Korea is being contacted regularly in Darwin, along with any number of JAs, with signals being as strong as ever heard on TE. The TE reports about 2000, and the signal is like this four nights out of five, with all districts except JA7 and JA8. Doug works quite a number on c.w. Plenty on s.a.h., but this mode still in the minority as yet in JA4.

Time is short with Doug for continuing much work with MS signals to David VK8AU at Tennant Creek, but reports the improvement in signals since installing half inch foam helix cable to the beam, which has a loss of 1.8 dB, per 100 feet at 1.8 GHz!

ACTIVITY IN CANBERRA

VKIDA reports there are about seven stations operational on the non-net sections of 52 MHz. The number has dropped since the netting of 52.53 MHz, but operation is spasmodic. On 144 MHz there are about five stations with tunable and portable equipment, but the contacts appear to be the skeds between Eddie VK1VP and Alec VK2AAK on 144.100 MHz. Ten c.w. stations operate on the 144.475 f.m. with regularity, plenty not so regular. Charlie VK1CR is working Sydney stations on Channel B with fair success most nights. Keith VK2AA is being contacted regularly on VK1, and the boys are beginning to wonder if anybody in Sydney operates in the lower parts of these bands.

Andrew reports it seems unlikely Canberra will have a repeater for the f.m. channels because it would not significantly improve the coverage of the stations in the Canberra area and would be a little help in increasing the coverage between mobiles in his area of the State. The locals therefore are more favourably orientated toward a beacon (excellent news—SLP) and present plans are to operate on 144.475 with 10w, output, solid state, turnstile or big-steel antenna, 5 seconds on, 5 seconds off, then 5 seconds of call sign in c.w., on an elevation a little above Canberra.

Finally, it is interesting to note the art of home building still comes to the fore in Canberra where at the recent Convention a competition for home-brew gear was won by Eddie VK1VP with a line up of varactor triplers and mixers (144 MHz. input, 1296 MHz. output), and Second Prize went to the team was Neil VK1ZT with a 1296 MHz. converter and home-brew dish antenna. Third a two-one transmission made by Greame VK1CIC with 52 and 144 MHz transmitters in the same unit with 6/40 final transmitters.

Brian VK9BB/4 writes from Atherton in North Queensland to say the paragraph in April "A.R." was incorrect in stating he had worked HL9WJ along with VK6s, SKK and 8AU. He has not been active on 6 metres since leaving New Guinea, but would be pleased to answer any queries from anyone regarding v.h.f. r.t.t.y., teletype, equipment, etc. To assist him in this and in the hope of fostering interest, with eyes across the border to other areas, write to John E. Dunkley, 9 Elva Ave., Pookra, S.A., 5095.

RTTY IN VK5

RTTY is a little different from the usual have been heard on 144 MHz. In VK5 for awhile now, and were finally tracked down to being r.t.t.y. being used by John VK5JE at Pookra. The following table lists the frequency and answer any queries from anyone regarding v.h.f. r.t.t.y., teletype, equipment, etc. To assist him in this and in the hope of fostering interest, with eyes across the border to other areas, write to John E. Dunkley, 9 Elva Ave., Pookra, S.A., 5095.

VHF RTTY NET

Further to the above, John has given a lot of thought to the establishment of an r.t.t.y. net and after discussion with others tenders the following table lists the frequency and keying (a.s.k.) as this is more suited to v.h.f. operation, and facilitates auto-start, etc., and receives a number of stations, more than f.a.s. as used on the lower bands. He recommends 144.630 MHz. as the net frequency, being located in some of the upper areas of the 2 metre band, and being a frequency which is free of other nets and beacons. (There has been such a net on 146.584 MHz. in VK3 for some two years or more.—Ed.)

METEOR SCAFTER

A little more news on this interesting phase of Amateur Radio. Wally VK3ZWV has been successful in establishing a net on 144 MHz. and VK2ZQJ via MS on 28th and 30th April at about 0615. Signals were considered good when only random meteor were being used, and the contacts were made good enough to record the efforts on tape. So that makes two States for Wally now by that mode. Also in on the act was David VK2GMO who heard Rod on 30th April. The story leading up to David's efforts arose from a comment following publication of the Contest announced last month by VK8AU when mention was made that only stations with elaborate equipment would get anywhere. Challenged to overhaul his own gear, David set about improving his receiving gear—the result—VK2ZQJ. So one never knows just what can be accomplished until you try; good luck David, you might join the ranks of

those making such contacts. Wally reports that around 0600 to 0700 is the best time, particularly for random scatter contacts. He would be pleased to answer any queries and to give it a go, as he is now on the path to attempting worked-all States via MS. A note from Wally VK3ZWV reveals there have been three known openings to JA during April, and stations were worked on two of these. He also has a tape recording of a contact received from HL9WJ in South Korea on 17th April on 50.100 between 1515 and 1545 hours, and the same station was heard again on 18th April. During the month of April, Wally was told JAZIIV had worked an LU3 on 18th April, but no further news of this at present.

576 MHz. NEWS

Bob VK3AOT stirred up some activity in VK5 576 MHz. over Easter. On Good Friday he worked Dennis VK3BDA at home at Mt. Waverley from Mt. Cowley, distance 83.5m. signals S 9 plus; this just being a new VK3 record on Saturday and Sunday were spent on the Grampians on Mt. William. The path to Melbourne was a poor one, signals to VK3BDA were S 7-8. During the month of April, two-way contact was made on 576 MHz. 5 x 4 both ways, 143 miles. On Sunday morning, Wally VK3ZWV was in portable to West's Surf, 30 miles south of Melbourne and was contacted at S9, giving ST in return. Distance 147.3 miles, a record. The previous VK3 record was held in 1961. Bob suggests this is a definite revival of interest in 576 MHz. (John VK5QZ, holder of the present Australian record on 576 is waiting for a challenge.)

Further news from Bob on the VK3 scene shows that the last of the series of field days for the season held during Easter attracted 11 record holders to the VK3 scene, and the longest contact was on 2 metres over 240 miles. It is good to see that a series of field days can be supported so well, and difficult to get many stations into the field in VK5 on one day a year!

Very elusive VK3 station, VK3ZRO in Deniliquin, is now trying 432 with Ian VK3ZDW, but so far no two-way QSO has been achieved. This may be a contact worth looking into by the 432 operators in VK5, giving them another State.

Continuing, Bob reports excellent 2 metre contacts from early April, when 10 stations from Mt. Gambier to Melbourne were contacted and giving some of the lower powered Melbourne boys their first VK3 contacts. Mt. Gambier signals were also heard in Wangaratta and Deniliquin. On Monday night, the Melbourne Night Owls Club members had to contend with a very strong wind, and VK3ZRO, the 2 metre beacon on Mt. Lofy, at S9, every one in Adelaide having gone to bed! VK6VE at Albany at the same time was S1, making it the fifth beacon in Mt. Gambier heard in Melbourne for the season. The excellent conditions extended themselves to 432 MHz. Colin VK3DK in Mt. Gambier had contacts with VK3ZDW, VK3ZBR and VK3YDJ. Also noted that Ron VK3AKC worked Kevin VK3ZAH on 1296 on 30th April.

As predicted in these notes awhile ago, this autumn was a time to keep a good ear on 52 MHz., and the period around Easter and the following months was a good time to try. A telephone call from John VK4ZTB in Brisbane gave me the first hint of something to come. The following is a good sign, as he was being heard in that city from Japan or over 1000 to seven hours, and considered the best openings since 1959. John also mentioned in his phone call that Bob VK3ZWV had been heard on a W2 on c.w. on 6 metres. A week or so later, John made another telephone call confirming that contacts were still being made in VK4, but this time nothing eventuated in VK5. Many thanks for your interest John, it was worth the effort.

As predicted in mind the privately sponsored V.h.f./U.h.f. Contest by David VK8AU to be held in July and details of which, appeared in the April issue of "A.R."

A new station is operating from Casey Base in Antarctica with call sign VK0PP and Phil VK0PP operating on 14.450 MHz. No other details available at this stage.

That's all the news for this month. Closing with this thought: "Someone has defined courtesy as a form of polite behaviour practised by civilised people when they have time." 73, Eric, VK1LF. The Voice in the Hills.

SOUTH EAST RATIO GROUP OF S.A. ANNUAL CONVENTION

will be held over the week-end

12th and 13th June, 1971

at MT. GAMBIER

Events will include 80 and 2 metre fox hunt, 2 metre hold and a skiff hunt, acrobatics, plus other novelties.

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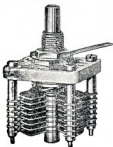
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CERAMIC MICRODENSERS ON 1-5/16" END-PLATE

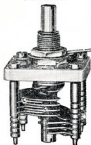
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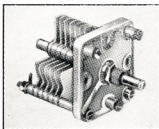
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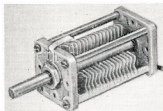


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TRANSMITTING VARIABLE CONDENSERS

Cat. No.	Type	Capacitance (pF.)		Proof Voltage	Air Gap (ins.)	No. of Vanes		Price
		Min.	Max.			Rotor	Stator	
815	Single Section	7.5	67	1,700	0.048	7	8	\$7.90
816	Single Section	9	192	1,000	0.024	10	9	\$8.18
817	Single Section	10	270	1,100	0.024	14	13	\$8.46



HIGH STABILITY TYPE

This pattern, Cat. No. 738, has double end-plates, 1-5/16 in. square, and double bearings, making it particularly suitable for high stability oscillator applications. Single section type, silver-plated finish. Max. Capacity: 93 pF.; Min. Capacity: 8 pF.; Air Gap: 0.03-in.; Proof Voltage: 1200.

Price \$7.81.

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CAPACITOR CATALOGUE



A comprehensive range of variable capacitors, well designed electrically and mechanically, and intended to stand up to continuous usage under all reasonable conditions. The types include single-section, split-stator, butterfly and differential capacitors.

Cat. No.	Type	Capacitance (pF.)		Proof Voltage	Air Gap (ins.)	No. of Vanes		Price
		Min.	Max.			Rotor	Stator	
478	180 deg. Split-Stator	3.25* 21	15 7.5	900 1,750	0.020 0.020	2*	2*	\$3.51
580	Single Section	4	13.5	2,300	0.062	4	4	\$3.73
581	Single Section	4	63	780	0.020	8	7	\$3.95
582	Single Section	4	63	850	0.020	8	7	\$3.88
583	180 deg. Split-Stator	4* 31	23 12	820 1,800	0.020	3*	3*	\$3.95
584	Butterfly	7* 41	32 18	970 1,740	0.020	8	7*	\$4.34
585	Single Section	4.5	91	780	0.015	11	10	\$4.51
586	Single Section	5	140	600	0.015	16	15	\$5.20
587	Butterfly	6	16	1,740 3,300	0.052	8	7*	\$4.83
588	Single Section	5	27.5	1,850	0.052	8	7	\$4.17
589	Single Section	5	60	1,000	0.030	11	10	\$4.51
719	Differential	3.25	25	950	0.020	4	5*	\$3.84
739	Butterfly	4.25* —†	10 —	2,000 3,700	0.052	5	4*	\$3.86

MINIATURE MICRODENSERS

Particularly suitable for VHF applications and where space is restricted. Robust construction. Two-hole fitting, using parts supplied.

Cat. No.	Type	Capacitance (pF.)		Proof Voltage	Air Gap (ins.)	No. of Vanes		Price
		Min.	Max.			Rotor	Stator	
551	Butterfly	4.5* 2.8†	26.5 14.5	500	0.01	10*	9*	\$3.73
552	180 deg. Split-Stator	3.5* 2.0†	21.5 11.5	500	0.01	4*	4*	\$3.63
553	Single Section	3.5	54	500	0.01	10	9	\$3.26

* Per Section.

† Series Gap.

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Sub-Editor: DON GRANTLEY
P.O. Box 222, Penrith, N.S.W., 2750
(All times in GMT)

It is very pleasing to note quite a large increase in the numbers of letters arriving at this QTH, most of which have been from the VK4 gang. Many thanks to all who have taken the trouble to write.

the following as worked on 20 max: FG7, PJ, KX5, OE, M1B Mario whose QSL manager is WAS7UP and whom I believe will QSL via the bureau; KX5, OE, M1B Mario whose QSL manager is WAS7UP and whom I believe will QSL via the bureau; K6G4C (via W2RDL), UKS, HA5, PJ5VR (Box 283, Curacao, Neth. Antilles), Y0, FBK, ZC4, 5348K (QSL to VET7WG), 0P8CK (who speaks on Genesee 1500), 1414Q (QSL to VP9, PF2GBG, QSL VE1DLZ), HC, CR4AJ, EA8, 5H3, 0A0, PZ3AA Willy (QSL to Box 100, 10000, Surinam or the bureau) John also works for Guyana, which is located in Zone 2 on Isachsen Isl. in North West Canada, 200m. south of Magnetic Nth. Pole and 600m. south of the Geographical North Pole.

HK0 suffix were K8HKB and W0KUS, and in each case the cards go to the home call.

Overseas Magazine Review

Compiled by Syd Clark, VK3ASC
and R. L. Gunther, VK7RG

FEEDBACK

Relevant to the review published in the April "A.R." for Ham Radio, Jan. 1971, I wish to defend antenna couplers I overlooked something important in WB2QGY's article, "Inexpensive SWR Indicator". I wish to comment on it here, because of some important principles involved.

In that article a primitive "SWR Meter" is supposedly obtained by a detector fed from a loop slipped around co-axial cable. The loop is run back and forth along the co-ax, supposedly to measure the distance between standing waves.

Unfortunately for this cunning idea, standing waves in a co-axial cable are confined to its inside surfaces. It is most dubious whether this can, as the author suggests, be reflected by a kind of leakage or induction from the surface of the braid—thereby to be picked up by his loop.

Any such outer-surface v.s.w.r. would be a function of tolerance and balance, with the principal consequences of distortion of the antenna pattern, and of radiation from (and pick-up by) the transmission line. The cure is simple: use suitable balun. This subject was discussed at length in 1969 issues of the "Australian EEB"—and so I certainly ought to have spotted the error.

It is not sufficiently appreciated that antenna matching involves two variables: matching the line to the antenna (or conversely), and matching the transmitter to the antenna. The latter is terminated in its characteristic impedance it will develop standing waves. As W5JJ has pointed out in recent Amateur literature (e.g. EEB April 1970), these will have relatively little consequence for v.s.w.r. less than 5:1 at frequencies less than 30 MHz. In terms of power loss, but they do complicate transmitter matching by presenting it with an indeterminate reactive load. Thus the usefulness of the antenna coupler becomes evident, which acts also to filter harmonics even in an ideally matched system.

Aside from the over-rated role of s.w.r. at h.f., the fact still remains that s.w.r. readings from a directional antenna bridge (or "SWR" bridge) can be misleading (as discussed widely during the past few years). In addition, optimum antenna-to-line matching depends on a deprecatingly large number of difficultly controllable variables—as discussed most interestingly in the October 1970 issue of "Spectrum" (N.Z.) in the article "SWR 1:1, Fact or Fiction".

The answer to proper antenna matching is, of course, the use of suitable instrumentation, i.e. the Antenna Noise Bridge (EEB Sept. 1969, "E.R." 12/70), v.f. bridge with slotted line ("E.R." 10/70), or "Antennascope" type of invariable r.f. bridge. (Orr Radio Handbook). See also comments in "Ham Radio" of November 1970 with a very interesting exchange between a correspondent and an author on the real meaning of reflected power—VK7RG.

AUSTRALIAN EEB

December 1970—

FET Conversion of BC221 Heterodyne Frequency Meter. I. N. Kallam, VK4. Useful information of great interest to those without instruction books.

A C-D Ignition with Automatic Changer. T. Vierz, VK4. Said to add zest to tired motor cars.

Commonsense Transmitter Loading. C. C. Drumeller, W5JJ. If your transmitter does not load properly, this is for you.

February 1971—

A Tachometer for Capacitor Discharge Ignitions. VK7KAR. More on "solid state" systems for motor vehicles.

A Nice Phase-Modulated Two Watt Tube Transmitter. L. Osborn. Small, neat and tidy.

Sythe-Stone Zener. T. M. Palmer, VK2. This worried me for a while and then I realised that I would spell it Sythe. It seems that recent worldwide sharpening shaves zener properties.

The Use of Avalanche Diodes. VK7RG. An interesting discussion of diodes and a means of checking unmarked units.

BREAK-IN

Jan.-Feb. 1971—

The Christchurch VHF Repeater. All valve job, neatly packaged.

R.S.G.B. Two Metre MOSFET Converter. ZL3TAU tells how they made this a V.h.f. Group project.

Solid State Check Check. ZL3TAT. Tells the user whether or not the transistor junction is okay or not. Naturally it also checks diodes. In or out of circuit, powered or unpowered.

March 1971—

Direct Reading Capacitance Meter. ZL2ADE. Reprint from "E.R." Apr. '70. Covers 0.10 pF. and 0.1 uF. in six ranges with linear scale. Accuracy claimed to be plus or minus 5%.

Transistor Checking with an Ohmmeter. ZL2AHP. Identifies the types, silicon or germanium, NPN or PNP and checks which lead is which.

Teletypewriter Equipment Speed Control Data. ZL2ALW. How you can do something about getting your teletypewriter operating at the correct speeds.

CQ

November 1970—

Electronic Keys—1970. WAMXK. Modern IC circuits of simple and laudible keys for use in keying transmitters. A 2N3440 transistor is used as the keying element. Stated to be suitable for Morse code keying.

The LSD (Lightweight, Study, Discone). An omnidirectional v.h.f./u.h.f. antenna. Reviews of Braks SFE-1000 Receiver, by W2AEF. Described as "a versatile solid state job for operation with a.m., s.b., c.w. or r.t.t.y. on 24 selected 500 KHz. segments in the range 1.8-30 MHz."

A Simple D.C. Voltage Dropper. W2FEZ. Using a six-volt tube recorder from a 12 volt battery.

Evaluation of the Decibel. Part 2, KBZB. The concluding article in a two-part series describing an every-day approach to understanding the "decibel".

Improving the Eloc 733 Transceiver. W3CWW. Some of these were sold in VK so there may be men who are interested. The power supply offers regulated r.t.t.y. output. The National NCX-A power supply is similar, but without the regulation.

December 1970—

A Solid State Comm. Receiver. I1TDJ. FET front using TIS34s, tunable i.f. on 3.5 MHz. followed by mech. filter i.f. on 250 KHz. Uses Common Gate circuit tuning.

Inexpensive Utility Antenna for 80 Mx. W6SAL. Simple certainly!

A Digitally Divided Frequency Standard for Lab. or Receiver. W7ZUL. Using four Motorola ICs, this unit gives outputs on 1 MHz., 100 KHz. or 25 KHz. and 5 KHz. Signals are stored on a readable scale at least 100 MHz.

In Defence of CW. W2EG. Should be read by all who feel that it should be dropped as a requirement for Amateur status.

Keyed Solid State Oscillators. Di Ming Lee. Transistors also drive the resonator for the drift are different and it can be minimised. Here's how!

An AZ-EL Antenna Mount for Satellite Tracking. Use W2AEP. Use two R.C.A. rotators, one on each axis. The rotators are sold here by R. H. Cunningham & Co. under the brand name "Stolle".

An FET RF Attenuator. W2EEY. A useful device to avoid receiver overload effects due to strong signals. One of the circuits in Fig. 2 locks a return path leaving the 5 to 9v. battery "up in the air".

Improving the Ham-M Rotor Indicator. by VK3KZ. The use of a solid voltage regulated supply keeps indications "on the beam".

January 1971—

QSK with the Heath SB-Series Equipment. K4JZ-CD. True QSK operation is not only desirable for low speed c.w. reg chewing, but is a must for fast, efficient traffic handling. Simple modifications enable such operation without sacrificing ease of operation in the s.b. mode.

F.M., KBSTH/3. An introduction to the joys and frustrations of FM operation is not only a must for all, but also a must for the serious.

Crystal Calibrators. How Solid is a Rock, K3STU. Understanding how to calibrate a calibrator and check it periodically, ensures that it will keep you where you want to be in the band of your choice.

The Mono-Loop Triband Quad. VK2AOU. Operating on 10, 20 and 40 m. and two element quad construction details.

Sunspot Cycle 20. Progress 1970. Prediction 1971. W3ASK. Enables you to decide the most productive times and arrange, in advance, to be there.

An Aural Diode Transistor Tester. W2EEY. This tester provides a simple aural indication of resistance values so one can concentrate on the components being measured without the interruption of having to examine a meter scale every time a test connection is changed.

February 1971—

An Introduction to VHF FM. Sub-titled "F.m. techniques for non-F.m.ers, W6HPH/G. F.m. offers several significant technical advantages over conventional a.m. and some over s.b. The author describes the merits of f.m. and the construction of two accessory devices to receive and transmit f.m. on the v.h.f. bands. F.M., KBSTH/3. Feature.

Calibrating FM Deviation. VE2AQX. Describes the Bestall Zero Method of calibration which is an absolute zero of modulation.

The Table Top Max. Linear. W6EL. A 3CX1000AT for 80, 40 and 20 metres.

OHM—The Oriental Ham Magazine

Nov.-Dec. 1970—

This is a rare title magazine which is published by Hong Kong and is usually filled with pictures and jottings about the goings on in Asia generally. This issue carries the news under the heading "A Good Job that Japan is likely to approve reciprocal licensing in the near future. No doubt this will boost her image."

Watch Those Cards. Z2MAZF. Discusses the problems of receiving cards from rare countries and methods of achieving the near impossible. Of course, if you are one of two or three who receive cards from these countries you might feel the problem is yours in coping with requests.

The technical content is "The GSKV" by G6W. Most Amateurs know this antenna quite well as it allows all band operation with one antenna from a location of limited extent. Do VKs know that GSKV is now VK3LV?

January 1971—

Electronic Keys. V5GAM describes a simple unit using a single transistor and about a dozen other components. Operation is from 9v. battery.

The balance of this issue is given over to stories of various happenings from here and there, mainly in the Orient.

QST

November 1970—

An Advanced General Coverage Amateur Receiver. W6BD. A very interesting specification of a receiver that still have stocks of tubes they wish to use.

160-80.75 Metre Broad Band Inverted Vee Antenna. W2PZY. Offers an analysis of how the system operates and shows how to construct a practical two band version of this effective antenna.

A VFO for 80 Through 10 Metres. Di Ming Lee. Here is an idea article showing how to use varactor and PIN diodes to tune and switch a variable frequency oscillator.

3-500W Grounded-Grid Amplifier for 50 MHz. W6GVF and W1HDP. Simple high power for owners of medium powered exciters.

A Station Control Unit for the Blind Amateur. W7ZUL. The first integrated control unit for the blind. With it the handicapped Amateur needs only rx, tx and antenna.

December 1970—

A Grounded-Grid MOSFET Receiver. by W7ZUL. Those of you who are seeking a modern design should be interested in this one. Single conversion, MOSFET mixer with 9 MHz. and 5.5 MHz. local oscillator using Common transistor components. A compact and sensitive receiver for 80 and 20 metres.

An Amateur Receiver for Aerial W2HG. Very useful for measurement of amplifier gain and other audio jobs.

Some Notes on the Design and Construction of a Grounded-Grid Linear Amplifier. W1KLE and W1ETU/4. If you have a spare 3-1000Z doing nothing you can put it to work. There is a second version using a pair of 3-500Zs for push-pull.

A Wide-Spread Multi-Element Tribander. W1FDY. Measuring 33 ft. 6 in. along the 20 m. band. It is a 20 m. band antenna and it is quite a lot for an antenna raising party to handle.

A High Output VFO for a Beginner's Transmitter. W3AEK. Output is on 3.5-4 and 7-7.5 MHz. Includes a 2w. amp. and broadband r.f. transformer. Solid state.

Midlatitude Intense Sporadic-E Propagation. W1GAE and W2BDC. Part 1. Causes and results. The result of observations made since the 1930s.

Recent Equipment: The Drake SP-4 Receiver, W1K/LK. 500 KHz. to 30 MHz. in bands 500 KHz. wide. In standard form it covers broadcast and international short wave broadcast bands. Obviously, if you wish to fit appropriate crystals it will cover any of the other segments also. I.F.s are on 5645 and 50 KHz.

January 1971—

Here Thoughts on Solid State Receiver Design, W2EJH. Here are some ideas which should interest the v.h.f. man who wishes to operate 10, 5 and 2 mX while using a single crystal. W1K/LK. The Kip-converting technique described in this article permits coverage of the h.f. bands from 160-15 mX plus WVV and provides birdie-free reception by using crystal resonators which fall above the tunable i.f. range of the main receiver.

Receiving F.M., W1K/LK. Part 1. Basic principles and circuits.

The Compact-A-Test, G5FP. A complete test instrument for the Amateur station.

The Morse-A-Verter, W7GHH/4. This device will make a teletypewriter to print characters at any speed from 5-50 words per minute from hand or machine sent Morse. All solid state. Seems to be a more practical item than the much older valve types which were offered commercially a few years ago. Mate one of these with a teletype keyboard type keyer and anyone could beat the code bogie.

Five for Five, K4ML. A simple two element "shortened LZ-Spectral" designed for a centre frequency of 14.15 MHz.

PEP, Average Power, and Related Matters, W4FB. Explains the meanings of the terms and how they are used.

Ham Radio Broadens Horizons for the Handicapped, W0QXA. Describes how many physically handicapped people can gain great benefit from Amateur Radio.

CW Communications for the Deaf, W2BKJ1. Describes a small device made by Western Electric to enable deaf people to know when they are being called by phone.

February 1971—

Quad v. Triband Yagi, W4FRU. Performance comparisons between these two popular antennas.

Cable and Easy Portable/Mobile Reception, W1CER. A new twist to converters, operating into a "squawk box".

Receiving F.M. Part 2 of W1K/LK's article. Describes several f.m. receiving adaptors for use with communications receivers and reviews a number of new f.m. discriminator designs. New designs include: M100, M101, M102, M103, M104, M105, M106, M107, M108, M109, M110, M111, M112, M113, M114, M115, M116, M117, M118, M119, M120, M121, M122, M123, M124, M125, M126, M127, M128, M129, M130, M131, M132, M133, M134, M135, M136, M137, M138, M139, M140, M141, M142, M143, M144, M145, M146, M147, M148, M149, M150, M151, M152, M153, M154, M155, M156, M157, M158, M159, M160, M161, M162, M163, M164, M165, M166, M167, M168, M169, M170, M171, M172, M173, M174, M175, M176, M177, M178, M179, M180, M181, M182, M183, M184, M185, M186, M187, M188, M189, M190, M191, M192, M193, M194, M195, M196, M197, M198, M199, M200, M201, M202, M203, M204, M205, M206, M207, M208, M209, M210, M211, M212, M213, M214, M215, M216, M217, M218, M219, M220, M221, M222, M223, M224, M225, M226, M227, M228, M229, M230, M231, M232, M233, M234, M235, M236, M237, M238, M239, M240, M241, M242, M243, M244, M245, M246, M247, M248, M249, M250, M251, M252, M253, M254, M255, M256, M257, M258, M259, M260, M261, M262, 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Amateur Radio, June, 1971



TWO METRE F.M.

from YAESU

FT-2F All Solid State TRANSCEIVER

Up-to-date advanced semiconductor techniques. 25 silicon transistors, 16 diodes, 1 SCR, 2 ICs, 1 FET.

The YAESU FT-2F opens the door to noise-free, broadcast quality two meter FM operation. And thanks to repeater stations in operation around the country, the two metre band is no longer limited to line-of-sight communications.

The FT-2F Transceiver is a highly advanced, all solid-state unit complete with an automatic tone-burst signal, with an on-off switch, for repeater actuation. The FT-2F has channel capability of 12 simplex or duplex frequencies. Three channel frequencies are included in the purchase price of the FT-2F. (Sets imported by B.E.S. will have simplex Ch. B and duplex (repeaters) Chs. 1 and 4 with crystals installed and aligned—six crystals.)

Advanced circuit design protects the rig automatically from the damage of transistors caused by antenna trouble, or reverse connection of the power line.

Nothing could be simpler than the operation of the FT-2F. Just select your channel and begin push-to-talk conversation with fellow two metre enthusiasts. A simple meter on the front panel indicates battery condition and relative power output. The meter automatically reverts to S meter operation in the receive mode.

Portable or home-base operation can be achieved with the addition of the optional FP-2 power pack. This AC power pack provides regulated DC power for the transceiver and charging voltage for optional leak-proof re-chargeable colloidal type batteries. In addition, a high fidelity elliptical style speaker is built into the pack. The FT-2F of course has its own self-contained speaker for independent use.

In the event of a disaster causing AC power failure, the FP-2 automatically switches over to DC operation from the battery pack. The battery pack will then provide up to eight hours of dependable emergency communications.

Like all YAESU Amateur gear, the FT-2F comes to you with our 90-day warranty. Plus all the hardware you need to get on the air immediately—mike, connectors, DC power cord and mobile mounting bracket. The special noise-cancelling microphone contains two dynamic inserts connected out of phase to shut off external noise.

If you have ever wanted to explore two metres, the time is NOW! And the rig is the YAESU FT-2F!

FT-2F SPECIFICATIONS

GENERAL:

Frequency Coverage: 144 to 148 MHz.
Number of Channels: 12 Channels (three supplied).
Modulation: Frequency Modulation.
Transmitter Control: Push-to-Talk.
Power Drain: Receives 0.5 amps., transmit 2 amps.
Power Source: DC 13.5 volts, plus or minus 10%.
Dimensions and Weight: 6½-in. w. x 2½-in. h. x 10-in. d.; 4 lbs.
Standard Accessories provided: Dynamic Microphone, Connector Plug, DC Cord—Fuse, Mobile Mount.

TRANSMITTER:

RF Output Power: 10 Watts (high position), 1 watt (low position).
Frequency Deviation: 15 KHz. maximum.
Frequency Stability: Plus or minus 0.001% or less.
Spurious Radiation: At least -60 dB. below Carrier.
Tone Burst: Nominal 2900 Hz.

FT-2F SPECIFICATIONS (continued)

RECEIVER:

Receiver Circuit: Crystal-controlled Double Conversion Superhet.
Intermediate Frequencies: 10.7 MHz. and 455 KHz.
Sensitivity: 0.3 uV, for 20 dB, S plus N/N Ratio.
Selectivity: Plus or minus 15 KHz. —5 dB.
Plus or minus 25 KHz. —30 dB.
Audio Output: 1 Watt.
Speaker: 2 inch Dynamic.

FP-2 AC POWER SUPPLY SPECIFICATIONS

Output: 13.5 volts, 2 amps.
AC Input: 100/115/220/234 volts, 50-60 c.p.s.
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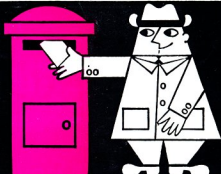
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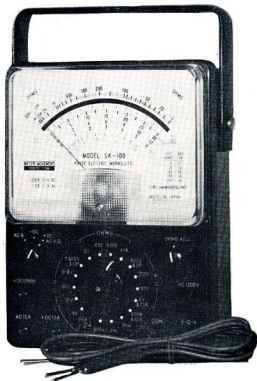
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